Depending upon the diode application, different models can be used. The simplest model is the *ideal diode* which looks like this.



In this model, if V<sub>d</sub> > 0, the diode acts as a zero resistance wire.
This model does find purpose as an *idiot* diode. An idiot diode is put in series with the power connections to protect circuitry from reverse polarity.



- ► A slightly more accurate diode mode is the piece-wise linear model.
- ► This model accounts for the forward voltage drop across the diode plus an equivalent resistance  $R_d$  equal to  $\frac{\Delta V_d}{\Delta I_d}$ , also known as the static diode resistance.



The schematic for this model would look like this:



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- A much more accurate model is a mathematical expression that has its origin from the physics point of view. This model is given by:  $I_d = I_s(e^{\frac{qV_d}{nkT}} - 1)$ ; where: n = 1.65 ideality factor varies with the diode  $I_s = 5 * 10^{-9}$  reverse saturation current  $q = 1.602 * 10^{-19}$  charge on an electron  $K = 1.38 * 10^{-23}$  Boltzmann's constant T = 300 absolute temperature
- ▶ k,T and q are constants, so  $\left(\frac{kT}{q}\right)$  is equal to ~26mV at 300K, so the equation can be written as:  $I_d = I_s \left(e^{\frac{V_d}{nV_T}} 1\right)$ ; where  $V_T$  is called the *thermal voltage*.
- ►  $I_s$  is on the order of  $10^{-9}$ , so it can be ignored relative to the exponential term, yielding:  $I_d = I_s(e^{\frac{V_d}{nV_T}})$

Using the mathematical model and data for a 1N4148 silicon diode, a Matlab plot of its IV characteristics looks like this:



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- Looking at the previous plot, we see a point with a given slope on the curve.
- The slope of the tangent line represents the dynamic resistance r<sub>d</sub> of the diode.



The slope of the tangent line r<sub>d</sub> is obtained by differentiation of the diode equation.

$$\begin{split} I_d &= I_s(e^{\frac{V_d}{nV_T}}) & \text{now, differentiate diode equation WRT } V_D \\ \frac{dI_d}{dV_d} &= I_s \frac{d}{dV_d} (e^{\frac{V_d}{nV_T}}) & \text{remembering: } \frac{d}{dx} a e^{ax} = a e^{ax} \\ \frac{dI_d}{dV_d} &= \frac{I_s}{nV_T} (e^{\frac{V_d}{nV_T}}) & \text{now, substitute } I_s(e^{\frac{V_d}{nV_T}}) \text{ for } I_d \text{ from first equation} \\ \frac{dI_d}{dV_d} &= \frac{I_d}{nV_T} & \text{now, invert both sides to obtain a resistance } \frac{V}{I} \\ \frac{dV_d}{dI_d} &= \frac{nV_T}{I_d} & \text{if } n=1, \ nV_t = 26mV, \text{ so since} \\ \frac{dV_d}{dI_d} &= r_d & \text{then...} \\ r_d &= \frac{26mV}{I_d} \end{split}$$

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*r<sub>d</sub>* is the model of the diode in the small signal condition. Its just a resistance with no voltage source.

The small signal diode resistance only applies for the condition where we are well beyond the barrier voltage 0.6V of the diode. Why?

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- When V<sub>d</sub> < 0V, the equation does not hold since we removed the I<sub>s</sub> term.
- Before we are a little past the threshold voltage, the exponential term will not dominate *I<sub>s</sub>*.
- A small signal condition is one where our signal amplitude is a small value in comparison with the other circuit voltages or currents.
- For example, a 100mVpp AC signal is a small signal with an amplifier that operates from 10V.