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Surface-normal plasmonic modulator using sub-wavelength metal grating on electro-optic polymer thin film



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ABSTRACT

In this work, we present the design, fabrication, and characterization of a surface-normal plasmonic modulator using sub-wavelength metal grating. The device consists of a 1.77 μ m efficiently poled electro-optic polymer film, which is sandwiched between a plasmonic grating and an indium–tin oxide film. A strong Fano resonance with a sharp plasmonic bandgap at 1522 nm wavelength was observed and electro-optical modulation was demonstrated based on the refractive index modulation of the polymer film. With future improvement in lowering the driving voltage and increasing the modulation depth, this hybrid organic/plasmonic modulator can readily expand into modulator arrays for three dimensional optical interconnects.

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1. Introduction

High speed Electro-optic (E-O) modulators have been identified as the key components in optical transceivers for communication systems [1–3]. Plasmonic modulators based on surface-plasmon polaritons (SPPs) will play pivotal roles in enabling nano-scale onchip photonics for high-density integration [4-10]. SPP based periodic metallic structures have been intensively investigated as active plasmonic devices in modulation applications, as they provide strong optical mode confinement, ultra-compact footprint, and active manipulation of photons [11-14]. In recent years, dynamic control over SPPs has been realized by modulating the refractive index of the dielectric layer adjacent to the metal surface [15,16]. Among the choices of the materials, E-O polymer possesses exclusive advantages such as large Pockels effect ($> 200 \ \text{pm/V})$, fast modulation speed and low dispersion across the RF to optical frequencies [17-21]. Further, polymers can be infiltrated into plasmonic structures, which allow the combination of the highly nonlinear optical effect of polymers with the strong field confinement of ultra-compact plasmonic structures. Recently, plasmonic/polymer hybrid waveguide modulators have been demonstrated, which are usually formed by uniform metal-dielectric

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http://dx.doi.org/10.1016/j.optcom.2015.04.058 0030-4018/© 2015 Elsevier B.V. All rights reserved. thin films or stripes [22–25]. However, such modulators only allow in-plane photon manipulation with high insertion loss.

In this work, we present the design, fabrication, and characterization of a surface-normal plasmonic/E-O polymer modulator that combines the merits of sub-wavelength metal gratings and efficiently poled E-O polymer thin film. The reported modulator structure possesses high optical confinement, low insertion loss, and is easy integrated with other optoelectronic devices for free-space 3-D optical interconnects [26,27].

2. Device structure

The configuration of the device is shown in Fig. 1(a), which consists of a gold (Au) /polymer/indium–tin oxide (ITO) sandwich structure on a glass substrate. A layer of 110 nm ITO film was deposited onto a 25 mm × 25 mm glass substrate using a two-inch ITO target (90% In_2O_3 , 10% SnO_2 by weight) in an AJA Orion 5 sputtering system. Substrate rotation was employed to ensure uniform film thickness. Deposition was performed at 75 W of RF power and a chamber pressure of 5 mTorr using 9.7 sccm of argon and 0.3 sccm of oxygen. Substrates were heated to 300 °C during the deposition. The ITO film thickness was measured on photolithographically patterned features using a Tencor Alpha Step 500 profilometer. The resistivity was measured to be 334 $\mu\Omega$ cm using a Jandel Multi Height Probe with a RM2 Resistivity Test Unit. The



Fig. 1. (a) Schematic illustration of the surface-normal plasmonic modulator. (b) Cross-sectional view of the device structure with geometric parameters.

ITO electrode was patterned and partially etched by hydrochloric acid in order to reduce the capacitance with the Au grating. The E-O polymer in this study is a guest-host polymer composite in poly (methyl methacrylate-co-styrene) (PMMA-co-PS) using AJLZ53 as one of most efficient and photo-stable dipolar tetraene chromophores at the loading level of 15 wt%. This polymer exhibits large E-O coefficient and high processing reliability in poled thin films, and has been used as a standard EO polymer with glass transition temperature (T_g) of 110 °C for the study of photonic devices [28]. Its thin film was prepared by spin-coating of formulated solution in dibromomethane onto the ITO substrate with a spin speed at 2000 rpm for 60 s, followed by overnight baking in vacuum oven at 65 °C to ensure complete removal of the residual solvent, leading to high optical quality films with thickness of 1.77 µm. The refractive index of the unpoled polymer films was measured by ellipsometry to be 1.571 at 1522 nm. A 100 nm Au thin film was deposited onto the polymer layer by thermal evaporation with a deposition rate of 8 Å/s. In order to reduce the RC delay of the device, a shadow mask was used to reduce the gold pad size. The key for enabling modulation is to create the Pockels effect in the E-O polymer sandwiched between the top Au and bottom ITO layers. This was achieved by generating the noncentrosymmetric order of nonlinear optical chromophores through poling process in presence of applied electric field. The E-O polymer was poled with contact poling method with E-O coefficient r_{33} of 71 pm/V as measured by the standard Teng-man reflective measurement system at 1300 nm [28,29]. The nanoscale slits were milled by focused-ion beams (FIB), with gallium ion energy of 30 kV and current of 10 pA. The periodicity of the grating was designed at 978 nm with the slit width of 100 nm, as shown in Fig. 1(b).

The key challenge faced in the fabrication process is precisely controlling geometrical dimensions and obtaining smooth slits at the Au/polymer interface. The ability to control the width of the gap and to minimize the fabrication defects is crucial for obtaining a sharp bandgap for the device. An optical image of the fabricated 53.8 μ m \times 53.8 μ m plasmonic grating structure after the FIB milling is shown in Fig. 2(a). A high-resolution scanning electron microscopy (SEM) image of the grating is shown in Fig. 2(b), which indicates the high quality of the grating structure with smooth slits in the presence of E-O polymer thin film.

3. Experiment and results

3.1. Simulation and experiment of Fano resonance

The Fano resonances in the sub-wavelength metal grating have been intensively investigated by many researchers [11-14]. Fig. 3 (a) shows the experimental setup of measuring the transmission spectrum. A broadband continuous wave laser (Thorlabs, S1FC1550) centered at 1550 nm was coupled into a fiber-based polarizer (Thorlabs, ILP1550SM-FC) to generate a linearly transverse magnetic (TM) polarized light with electric field polarized perpendicular to the slit direction (along x axis in Fig. 2). The output light was then collimated through a $40 \times$ objective lens (NA=0.65). The diameter of the collimated beam is about 130 μ m. A 50 µm pinhole was used in front of the modulator to block the excessive light of the collimated beam before coupling to the device in order to obtain the coupling efficiency to the SPP mode. The device was mounted on a five axis stage, which allowed precise adjustment of the position as well as the incident angle within 5×10^{-5} rad. The transmitted beam after the sample was focused by a $40 \times$ objective lens and coupled into an optical spectrum analyzer (Thorlabs, OSA203B) with a standard SMF-28 fiber.

Fig. 3(b) shows the measured and simulated transmission spectra with a wavelength range from 1450 nm to 1600 nm. The simulation is based on Rigorous Coupled Wave Analysis (RCWA) in DiffractMod of RsoftTM. The transmission spectra, indicate the asymmetric lineshape of the Fano resonance with a sharp transition edge. The resonance is attributed to the coupling of the discrete guided modes induced by Bragg-grating-modulated SPPs with the Fabry-Perot (FP) resonance in the narrow slits and waveguide mode resonance in the polymer layer [11,12]. The location of the transmission maximum agrees with the simulated curve, as shown in Fig. 3(b). Our experimental results show that the total transmitted optical power is 23%, which is 6.3 dB insertion loss. In our simulation in Fig. 3(b), the structure shows 43% of normalized transmission at the resonance peak, where the loss is determined by the combined loss from the metallic grating and the absorption from the ITO film. The optical loss of the 100 nm ITO thin film was measured to be 1.1 dB at 1528 nm. From the experimental results, it can be concluded that the coupling of the light to the SPP mode of the plasmonic grating shows a loss of 5.2 dB. The reduced peak intensity and broadening of the spectrum compared with simulation results are attributed to the non-perfect collimation, the edge roughness from the FIB process, and the ohmic loss of the Au thin film. The resistivity the 100 nm Au thin film was measured to be $4.08\times 10^{-8}\,\Omega$ m, which is nearly two times higher than bulk Au resistivity [30]. Fig. 3(c) and (d) shows the cross-sectional views of the electric field distribution $|E/E_0|$ (where E_0 is the electric field amplitude of the incident light) associated with the SPPs at the Au-polymer interface at 1522 nm along the z-axis and x-axis, respectively with no applied voltage. The enhanced E_z extend into the polymer layer, as shown in Fig. 3(c), resulting in overall $3 \times$ electric field amplitude enhancements over a large volume in the polymer layer, which has very good overlap with the modulating electric field induced by the vertical electrodes. Fig. 3 (d) indicates extraordinary transmission effects in the narrow slits.

3.2. Demonstration of electro-optical modulation

In order to investigate the E-O modulation due to the Pockels effect of the polymer layer, a 20 V DC voltage was applied between the grating and the grounded ITO layer. The change of the refractive index Δn can be written as [31]

$$\Delta n = -\frac{1}{2}n_{\rm e}^3 r_{33} \frac{V}{d} \tag{1}$$



Fig. 2. (a) Optical microscopy and (b) SEM images showing the fabricated sub-wavelength metal grating.

where *V* is the applied voltage and *d* is the polymer film thickness. The extraordinary refractive index n_e of the poled films is 1.61 measured by Metricon 2010 prism coupler. Considering the results that r_{33} is 71 pm/V at 1300 nm corresponds to 60 pm/V at 1522 nm based on the two-level approximation [32], Δn was calculated as 0.0014. The wavelength of the Fano resonance is determined by the periodicity of the structure *p*, Au permittivity ε_{Au} , and the polymer permittivity ε_d , which can be explained by the SPP zero-order relation [33]:

$$\lambda_0 = n_{\rm spp} p, \tag{2}$$

$$n_{\rm spp} = \operatorname{Re}\left(\sqrt{\frac{\varepsilon_{\rm Au}\varepsilon_{\rm d}}{\varepsilon_{\rm Au} + \varepsilon_{\rm d}}}\right) \tag{3}$$

The simulation curves in Fig. 4 indicate a wavelength shift occurs due to the small change of polymer index Δn of 0.0017 in the presence of the applied voltage. With a probing wavelength of 1522 nm, the simulated transmission spectra show that a very small index modulation of 0.0017 induces the decrease of the optical transmission from 17.5% to 12.6%. Fig. 4 also shows experimental results of the wavelength shift with an external 20 V voltage applied. The measurement curves show that the optical transmission drops from 15.3% to 14.1% at 1522 nm. The discrepancy between the experiment and simulation possibly result



Fig. 4. The simulation and experimental curves showing the spectrum shift under 20 V voltage.

from the degradation of the polymer E-O efficiency r_{33} in the grating region after the FIB process. Due to the small thermal conductivity of polymers [34], FIB heating could induce thermal relaxation of poled films to certain extend, and therefore the r_{33} value of the grating region (53.8 µm × 53.8 µm) is degraded compared to the measured value using the Teng-man method with a large collimated beam size (2.6 mm × 2.6 mm). Thin film E-O measurement proves that poled films, after being exposed to



Fig. 3. (a) Experimental setup for optical transmission spectrum. (b) The simulation and experimental curves showing the optical transmission spectrum. The electric field distribution along (c) z direction and (d) x direction at 1522 nm.



Fig. 5. Electro-optical modulation of the Fano resonance: lower curve is the driving electric signal, and upper curve is the responding optical signal.

thermal excursion at 60 °C for 15 minutes, retains about 70% of its initial r_{33} values. From the experimental result of wavelength shift in Fig. 4, the change of the refractive index was estimated to be 0.00063, which results in an in-device r_{33} of 27 pm/V at 1522 nm based on Eq. (1). The change of the optical field distribution at the probing wavelength induced by the modulation of the dielectric layer refractive index can be found in Refs. [11–14] and our previous work in Ref. [16].

A tunable laser (HP 8168 A) at 1522 nm was used in order to characterize the E-O modulation. An InGaAs photodetector was connected to an oscilloscope in order to monitor the transmitted optical power. The photocurrent is directly converted to voltage output through the 50 Ω impedance of an oscilloscope without any amplifier. A 1 kHz sinusoidal wave (20 V peak-to-peak) was applied to the device from a function generator (Wavetek, Model 395). The output of the optical signal in response to the electric driving signal is shown in Fig. 5. The modulation depth, which is the amplitude of the modulation voltage divided by the reference signal, only achieves 7.2% in our experiment, however, it is highly possible to obtain large E-O modulation (>50%) by using more efficient ($r_{33} > 200 \text{ pm/V}$) E-O polymers with higher thermal stabilities. The frequency response of our structure is limited majorly by the capacitance of the device, which is 260 pF measured at 100 k Hz. The relatively large capacitance is attributed to large gold pad size (3 mm \times 3 mm). Future work will also be focused on optimizing the FIB fabrication condition to obtain sharper transition edge of the Fano Resonance, which will increase the modulation depth. Modulation with lower driving voltage can be achieved by decreasing the thickness of the E-O polymer layer [35]. By these optimizations in design and fabrication, it would be possible to reduce the driving voltage to $\sim 1 \text{ V}$ and achieve a modulation depth of ~3 dB.

4. Conclusion

In conclusion, we have designed and fabricated an electrically driven surface-normal plasmonic/E-O polymer modulator that is suitable for 3-D optical interconnects. Due to the extraordinary transmission, the hybrid plasmonic/polymer device exhibits a Fano resonance with a sharp transition edge. The E-O effect in the polymer film enables modulation of the Fano resonance. Further improvements of the modulation performance will be focused on optimization of the poling process, decreasing the polymer thickness with more efficient and thermally stable E-O polymers, and improving the FIB fabrication, which will lead to an ultra-compact device with fast modulation and low driving voltage. Such surfacenormal plasmonic modulators are expandable to 2-D arrays, and can be integrated with energy-efficient optoelectronic driving circuits and low-cost continuous-wave vertical surface-emitting lasers towards the realization of out-of-plane optical interconnects.

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