

# SECTION 2: FIRST-ORDER FILTERS

ENGR 202 – Electrical Fundamentals II

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# Introduction

# Filters

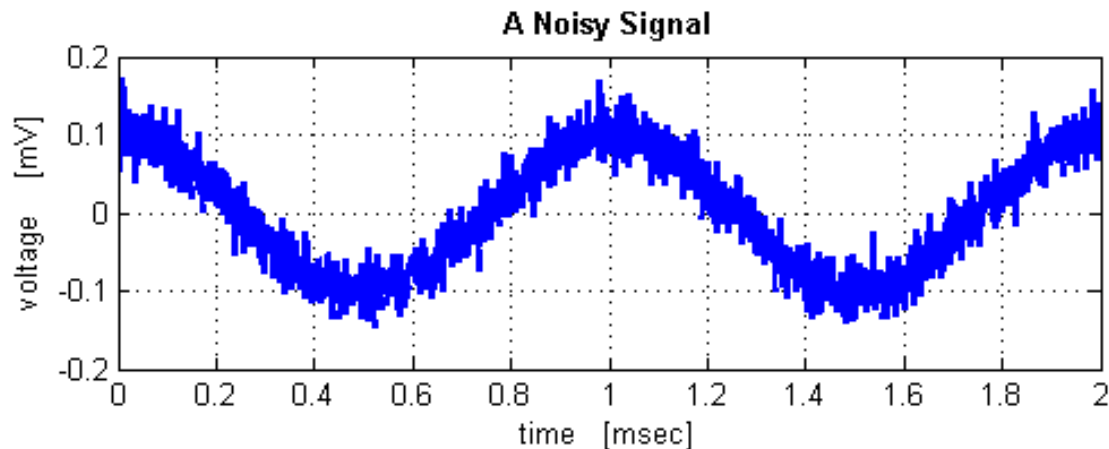
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- We are all familiar with ***water*** and ***air filters***
  - ▣ Basis for operation is ***size selectivity***
    - Small particles (e.g. air or water molecules) are allowed to pass
    - Larger particles (e.g. dust, sediment) are not
  - ▣ Unwanted components are ***filtered out*** of the flow.
  
- ***Electrical filters*** are similar
  - ▣ Basis for operation is ***frequency selectivity***
    - Signal components in certain frequency ranges are ***filtered out***
    - Signal components at other frequencies are allowed to pass

# Noise

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- All real-world electrical signals are *noisy*
  - ▣ You've seen this in the lab
  - ▣ Zoom in closely on a low-amplitude sinusoid with the scope (even one supplied directly from the function generator) – it won't look like a perfectly clean sinusoid



# Noise

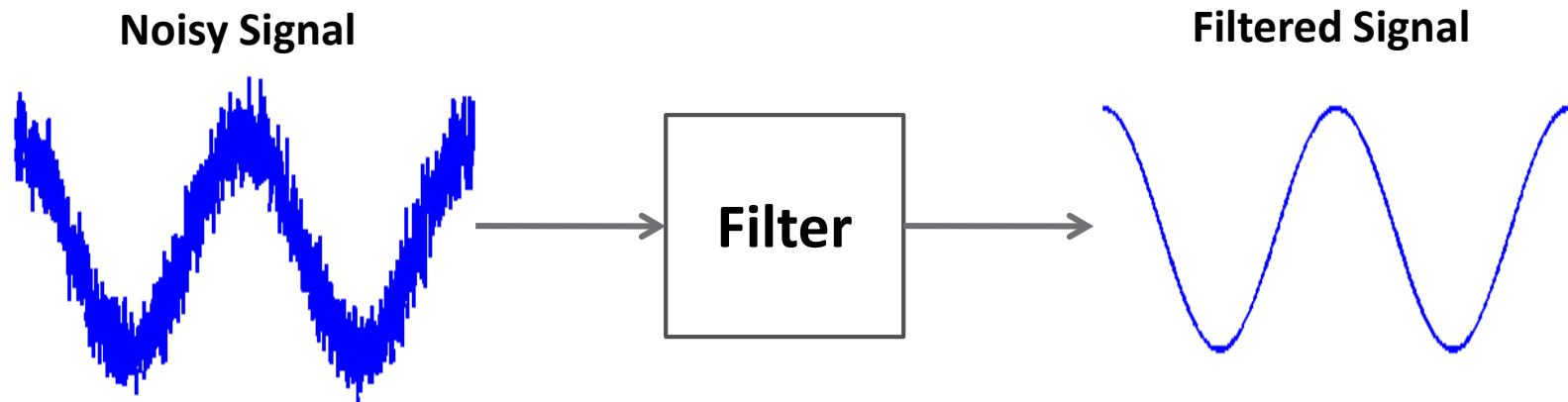
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- We will use the term ***noise*** to mean any electrical signal that interferes with or corrupts a signal we are trying to measure.
- Noise has many sources:
  - ▣ Measurement instruments themselves
  - ▣ 60Hz power line interference
  - ▣ Electrical components – resistors, transistors, etc.
  - ▣ Wireless LAN, fluorescent lights, computers, etc.
- We'd like to be able to remove, or filter out, this noise
  - ▣ Improve the accuracy of measurements
  - ▣ Often possible, if we know the ***frequency characteristics*** of the signal and the noise

# Filtering Noise

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- We'll learn how to design filters to remove noise



- First, we must introduce two important concepts:
  - ▣ ***Frequency-domain representation of electrical signals***
    - What is meant by “frequency characteristics” of an electrical signal?
  - ▣ ***Frequency response of linear systems***
    - How does a linear system (e.g. a filter) behave as a function of frequency?

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# Frequency Spectrum

# Frequency Domain

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- We are accustomed to looking at electrical signals in the ***time domain***
  - ▣ Amplitude plotted as ***function of time***
  
- Can also be represented in the ***frequency domain***
  - ▣ Amplitude plotted as a ***function of frequency***
  - ▣ ***Frequency spectrum***
    - Describes the ***frequency content*** of a signal
  - ▣ Can think of signals as a sum of different frequency sinusoids
    - What frequencies (sinusoids) are present



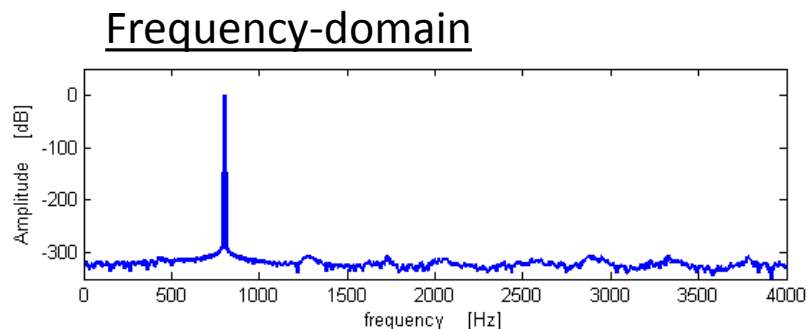
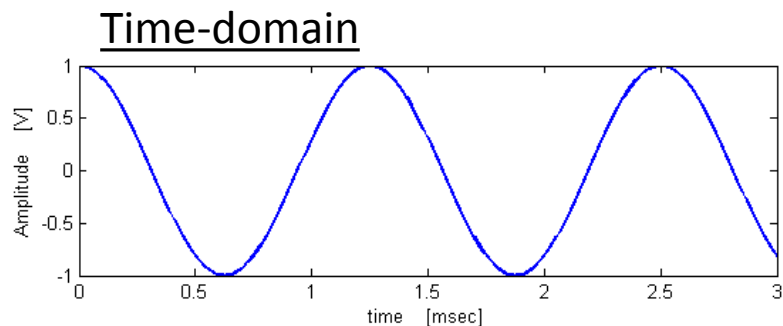
# Frequency Spectrum

- ***Frequency spectrum***
  - An ***amplitude vs. frequency*** plot
  - X-axis is frequency – not time
  - Y-axis is amplitude
  - Amplitude units may be in ***decibels (dB)***
  
- Shows the relative amount of energy at each frequency
  
- Time-domain plot and frequency spectrum are alternate representations of the same signal

# Frequency Spectra – Examples

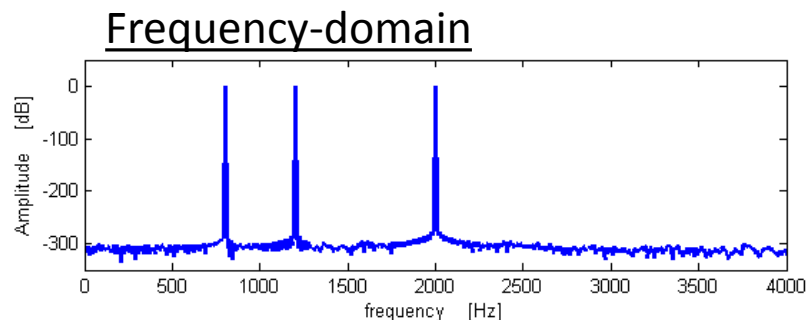
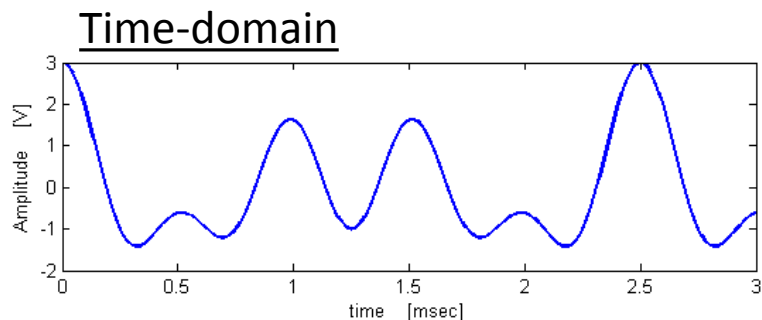
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- Single sinusoid:  $v(t) = 1V \cos(2\pi \cdot 800Hz \cdot t)$



- Sum of three sinusoids:

$$v(t) = 1V[\cos(2\pi \cdot 800Hz \cdot t) + \cos(2\pi \cdot 1200Hz \cdot t) + \cos(2\pi \cdot 2000Hz \cdot t)]$$

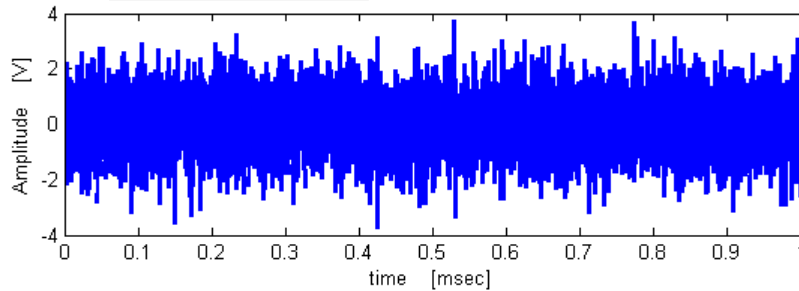


# Frequency Spectra – Examples

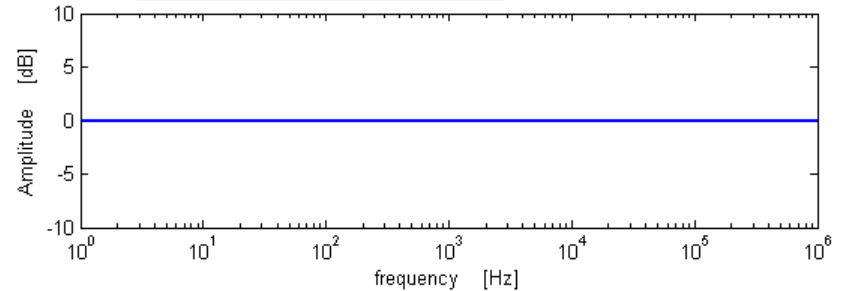
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## □ White noise:

Time-domain

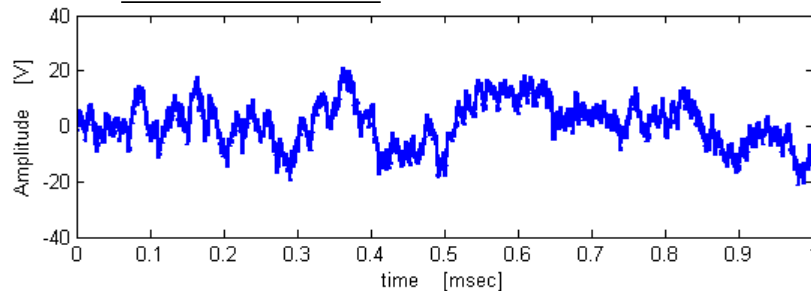


Frequency-domain

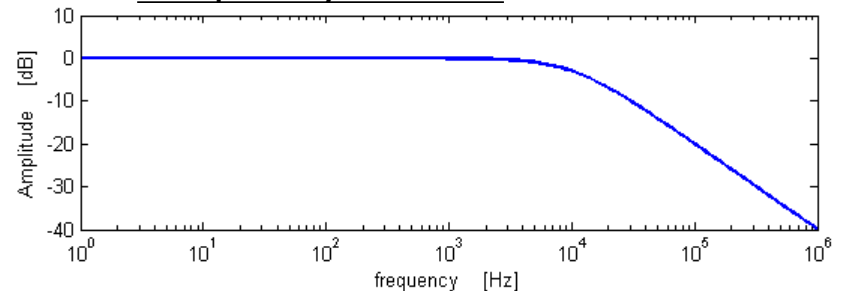


## □ Band-limited (colored) noise:

Time-domain



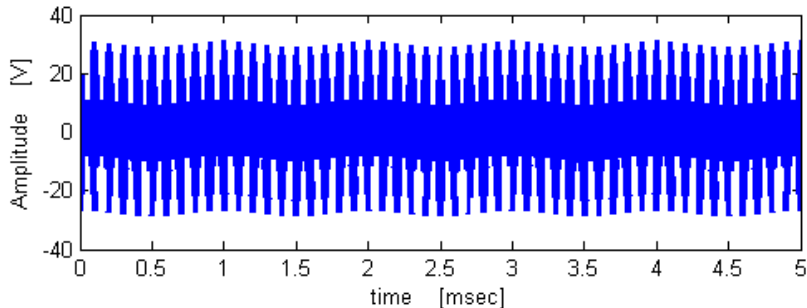
Frequency-domain



# Frequency Spectra - Examples

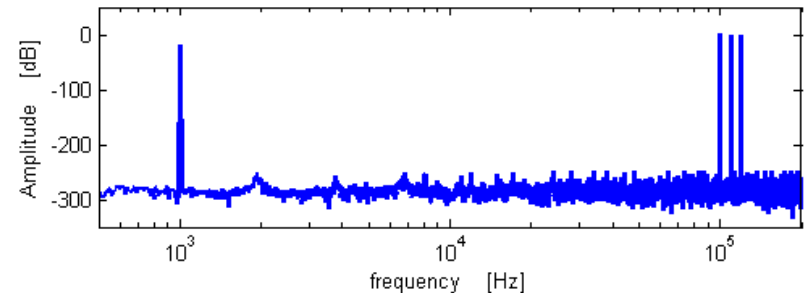
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- Consider the following scenario
  - ▣ Measuring a sensor output in the lab
  - ▣ Know the signal is roughly sinusoidal
  - ▣ Suspected frequency:  $\sim 1$  kHz

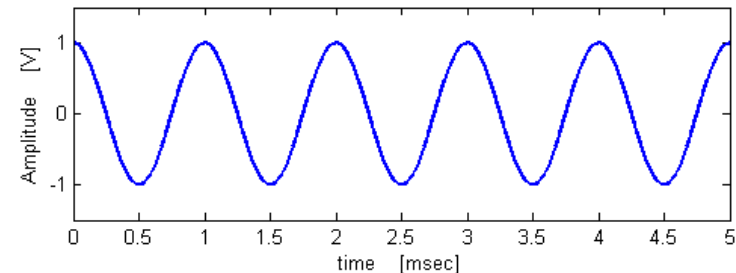


- Measured signal corrupted by noise/interference
  - ▣ Difficult to identify the interfering signal from the time-domain plot

- Same signal in the frequency domain:



- Three interfering tones
  - ▣ All near 100 kHz
- Can now design a filter to remove the noise:



# Fourier Transform

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## □ **Fourier transform**

- Transforms a time-domain representation to a frequency spectrum

$$V(\omega) = \int_{-\infty}^{\infty} v(t) e^{-j\omega t} dt$$

## □ **Inverse Fourier transform**

- Transforms from the frequency domain to the time domain

$$v(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} V(\omega) e^{j\omega t} d\omega$$

## □ A mathematical transform

- Two different ways of looking at the same signal
- A ***change in perspective*** not a change of the signal itself

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# Frequency Response of Linear Systems

# Frequency Response Function

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- Linear systems (electrical, mechanical, etc.) can be described by their ***frequency responses***
- Frequency response
  - ***Ratio of the system output phasor to the system input phasor***
  - In general, a ***complex function of frequency***

$$H(\omega) = \frac{\mathbf{Y}}{\mathbf{X}} = \frac{\mathbf{Y}(\omega)}{\mathbf{X}(\omega)}$$

- Complex-valued – has both magnitude and phase
  - Magnitude: ratio of output to input magnitudes
    - ***Gain*** of the system
  - Phase: difference in phase between output and input
    - ***Phase shift*** through the system

# Frequency Response – Bode Plots

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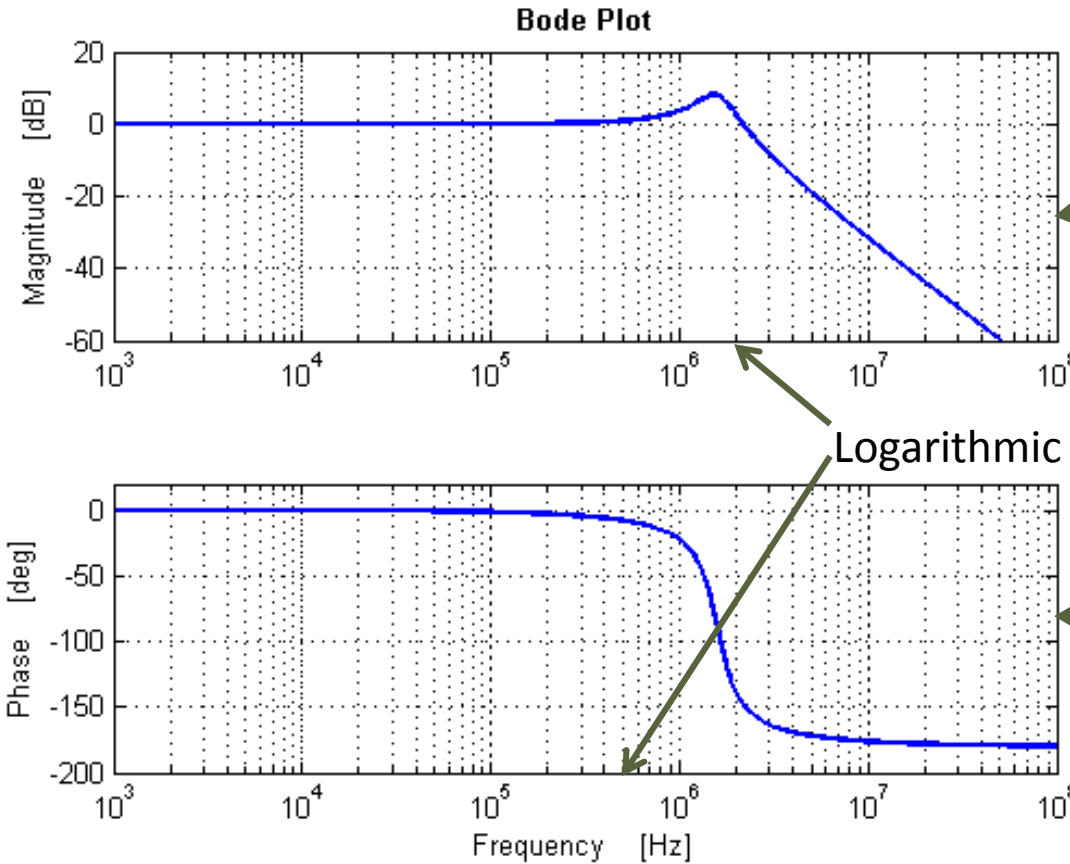
- ***Frequency response***
  - Description of system behavior *as a function of frequency*
  - ***Gain*** and ***phase***
  
- Represented graphically – formatted as a ***Bode plot***
  - Magnitude plot on top, phase plot below
  - Logarithmic frequency axes
  - Magnitude usually has units of decibels (dB)
  - Phase has units of degrees



# Bode Plots

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Units of magnitude are dB



Magnitude plot on top

Logarithmic frequency axes

Units of phase are degrees

Phase plot below

# Decibels - dB

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- Frequency response gain most often expressed and plotted with units of ***decibels*** (dB)
  - A ***logarithmic*** scale
  - Provides detail of very large and very small values on the same plot
  - Commonly used for ***ratios*** of powers or amplitudes
- Conversion from a linear scale to dB:

$$|H(\omega)|_{dB} = 20 \cdot \log_{10}(|H(\omega)|)$$

- Conversion from dB to a linear scale:

$$|H(\omega)| = 10^{\frac{|H(\omega)|_{dB}}{20}}$$

# Decibels – dB

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- Multiplying two gain values corresponds to adding their values in dB
  - ▣ E.g., the overall gain of cascaded systems

$$|H_1(\omega) \cdot H_2(\omega)|_{dB} = |H_1(\omega)|_{dB} + |H_2(\omega)|_{dB}$$

- Negative dB values corresponds to sub-unity gain
- Positive dB values are gains greater than one

dB	Linear
60	1000
40	100
20	10
0	1

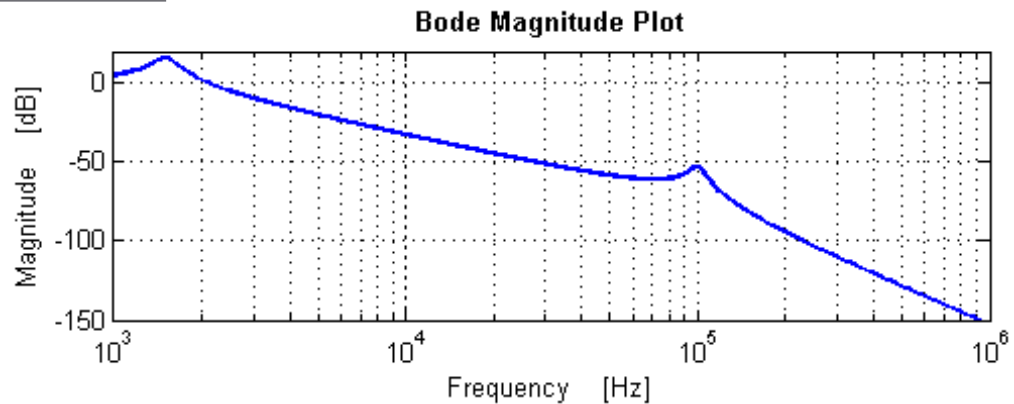
dB	Linear
6	2
-3	$1/\sqrt{2} = 0.707$
-6	0.5
-20	0.1

# Value of Logarithmic Axes - dB

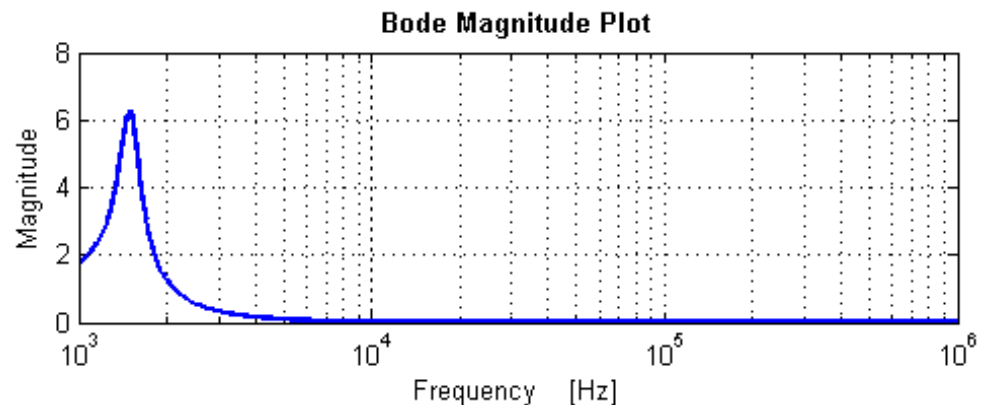
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- Gain axis is linear in dB
  - ▣ A logarithmic scale
  - ▣ Allows for displaying detail at very large and very small levels on the same plot

- Gain plotted in dB
  - ▣ Two resonant peaks clearly visible



- Linear gain scale
  - ▣ Smaller peak has disappeared

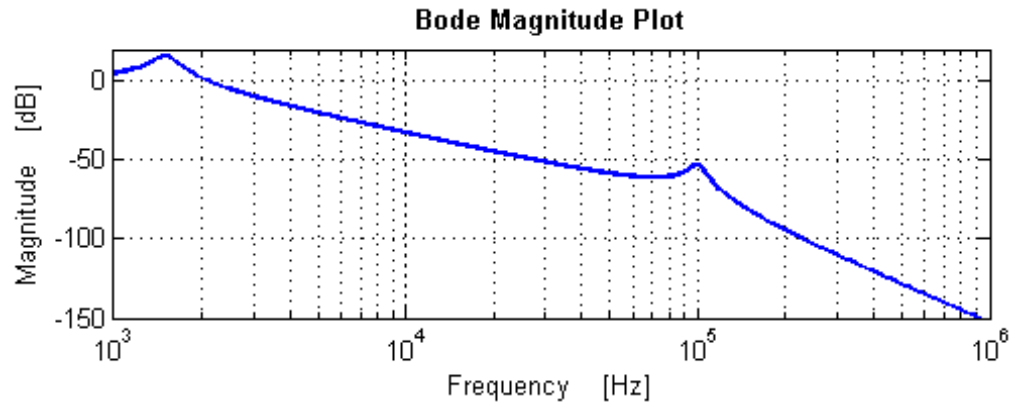


# Value of Logarithmic Axes - Frequency

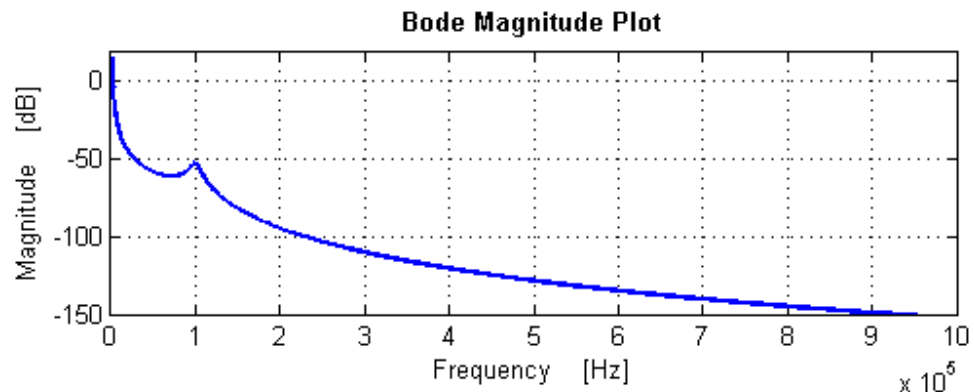
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- Frequency axis is logarithmic
  - ▣ Allows for displaying detail at very low and very high frequencies on the same plot

- 
- Log frequency axis
    - ▣ Can resolve frequency of both resonant peaks



- 
- Linear frequency axis
    - ▣ Lower resonant frequency is unclear

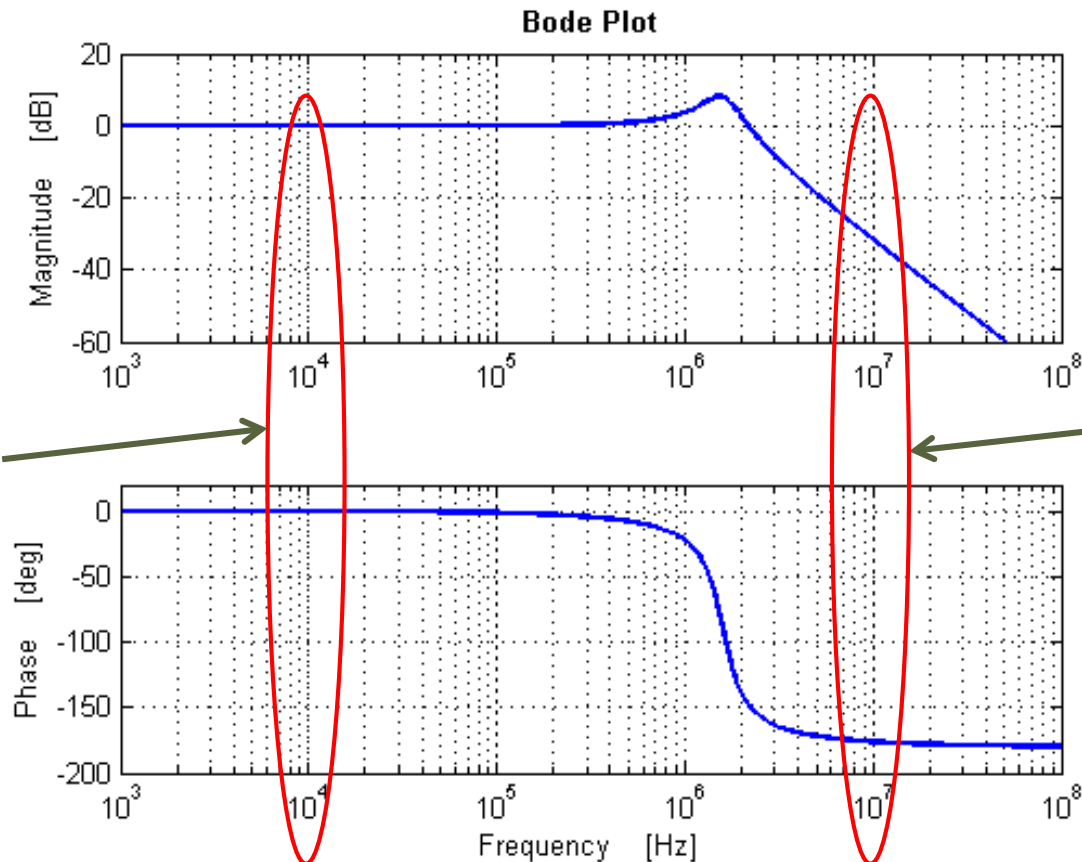


# Interpreting Bode Plots

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**Bode plots tell you the gain and phase shift at all frequencies:**  
choose a frequency, read gain and phase values from the plot

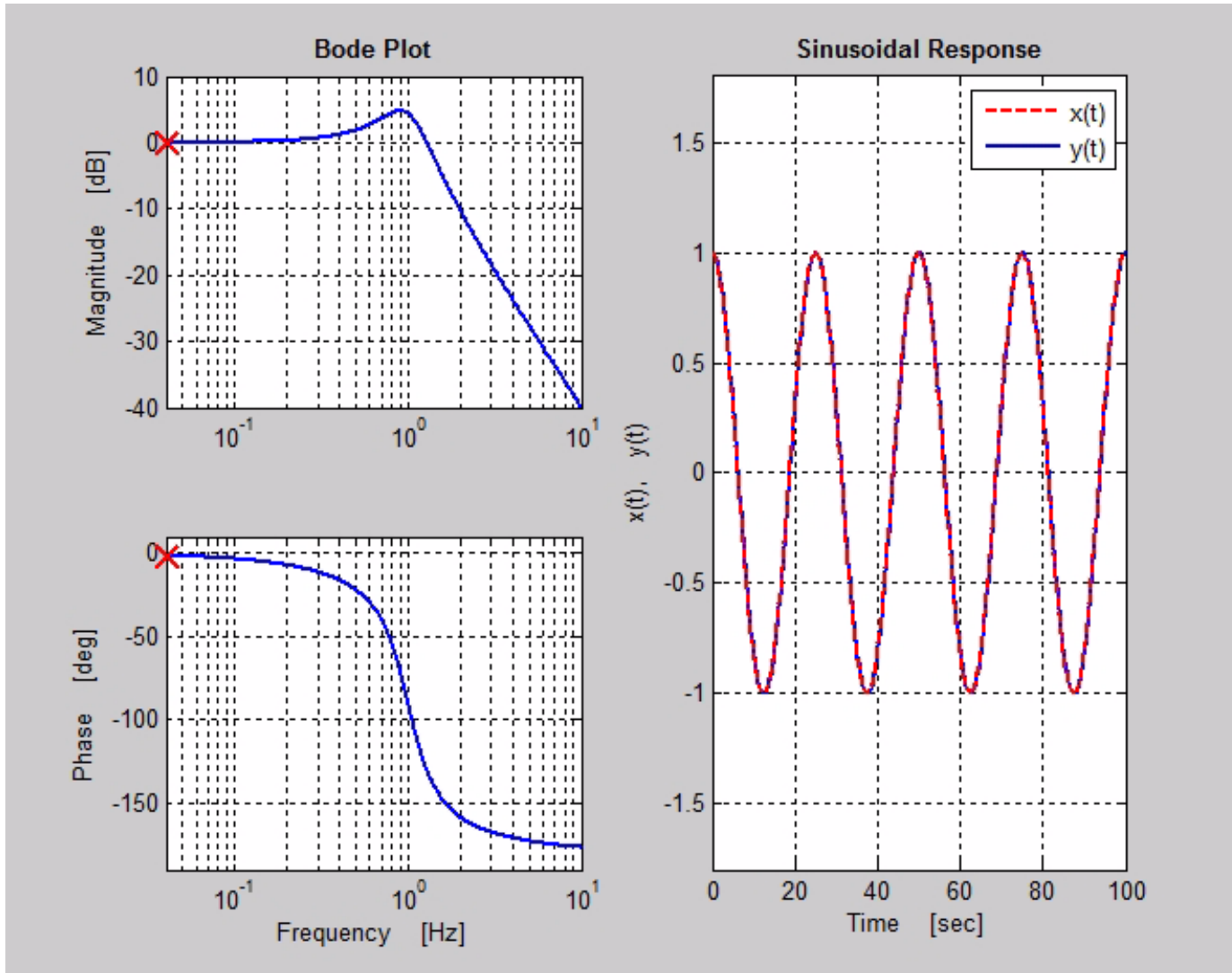
For a 10KHz sinusoidal input, the gain is 0dB (1) and the phase shift is  $0^\circ$ .



For a 10MHz sinusoidal input, the gain is -32dB (0.025), and the phase shift is  $-176^\circ$ .

# Interpreting Bode Plots

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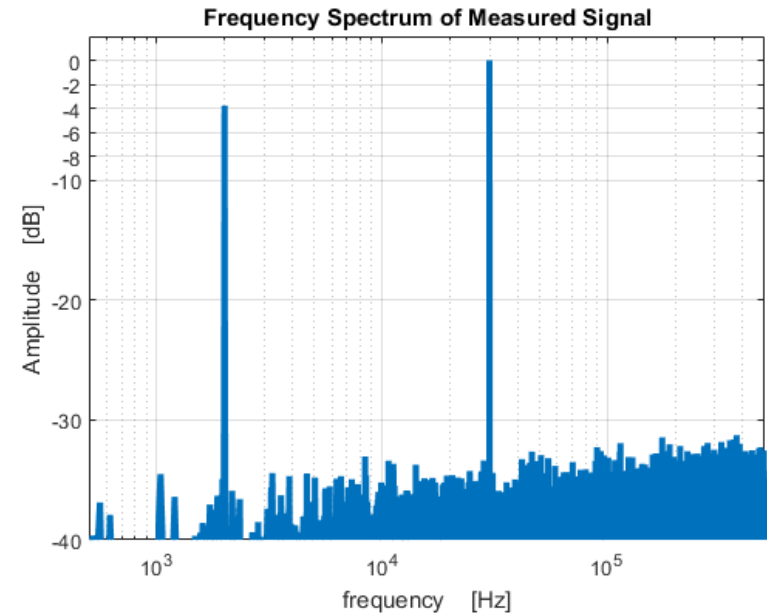


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# Example Problems

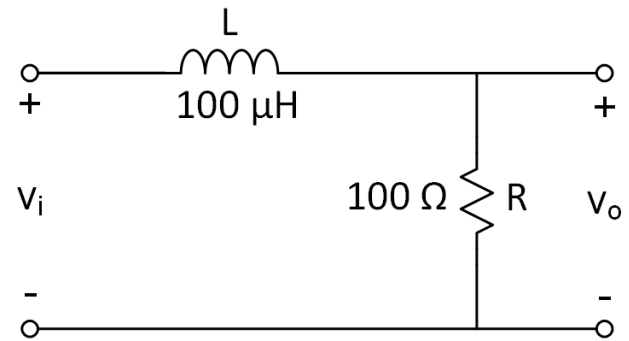


A measured signal has the frequency spectrum shown here. Assuming the larger signal component has an amplitude of 500 mV, and that both signal components are in phase, write a time-domain expression for the measured signal.



Determine the frequency response function,  $H(\omega)$ , for the following circuit.

What are the circuit's gain and phase at 200 kHz?

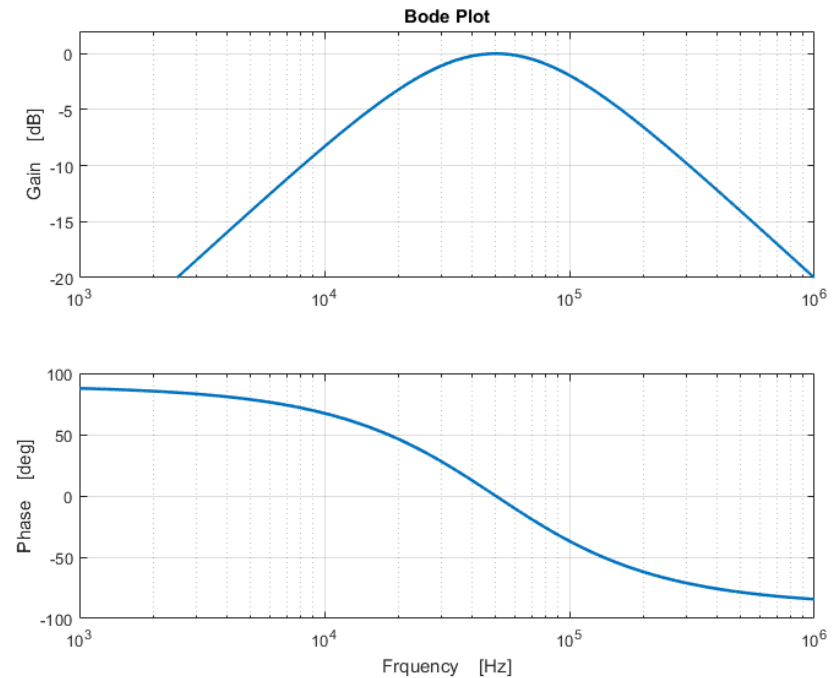




The input to a circuit with the following Bode plot is

$$v_i(t) = 1.2V \cdot \cos(2\pi \cdot 10kHz \cdot t)$$

What is the output,  $v_o(t)$ ?



# Types of Filters

Filters are classified by the ranges of frequencies they pass and those they filter out

# Filter Operation

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- ***Frequency spectrum*** describes frequency content of electrical signals
- ***Frequency response*** describes system (circuit) gain and phase at different frequencies
- Can design circuits (i.e. ***filters***) to have high gain at desirable frequencies and low gain at undesirable frequencies
  - Want to filter out high frequencies?
    - Design a filter with low gain at high frequencies and high gain at low frequencies.
  - Want to filter out all signals between 1 MHz and 10 MHz?
    - Design a filter with low gain in this range and high gain everywhere else.

# Types of Filters

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- Filters are classified according to the ranges of frequencies they pass and those they filter out
  - **Low pass filters:** pass low frequencies, filter out high frequencies
  - **High pass filters:** pass high frequencies, filter out low frequencies
  - **Band pass filters:** pass only a range of frequencies, filter out everything else
  - **Band stop (notch) filters:** filter out only a certain range of frequencies, pass all others

# Ideal Filters

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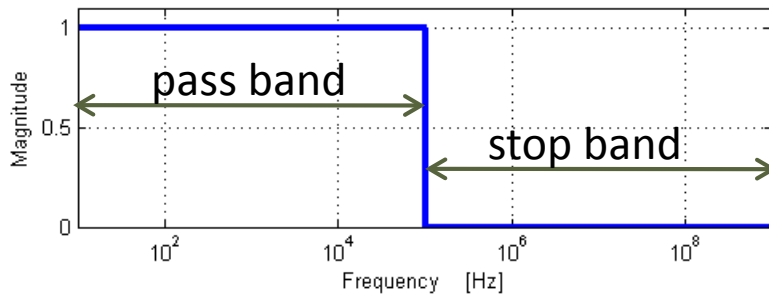
- ***Ideal filter*** gain characteristics:
  - ***Unity gain*** in the ***pass band***
    - Range of frequencies to be passed
  - ***Zero gain*** in the ***stop band***
    - Range of frequencies to be filtered out
  - ***Abrupt transition*** between pass band and stop band
- Signals with frequency components in the pass band pass through the filter unaltered
- Signals with frequency components in the stop band are completely filtered out – removed from the signal



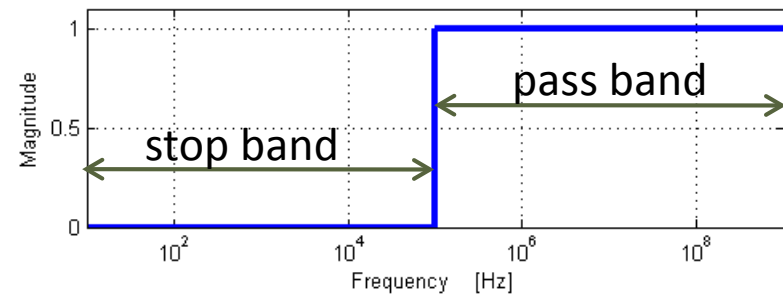
# Ideal Filters – Magnitude Response

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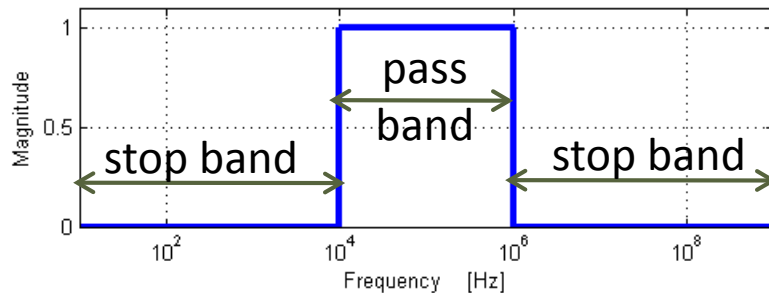
**Ideal Low Pass Filter**



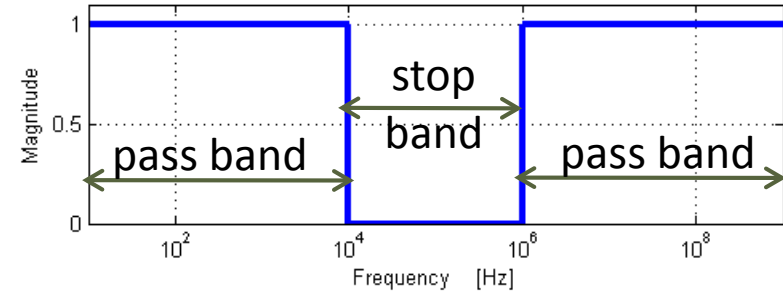
**Ideal High Pass Filter**



**Ideal Band Pass Filter**



**Ideal Band Stop Filter**



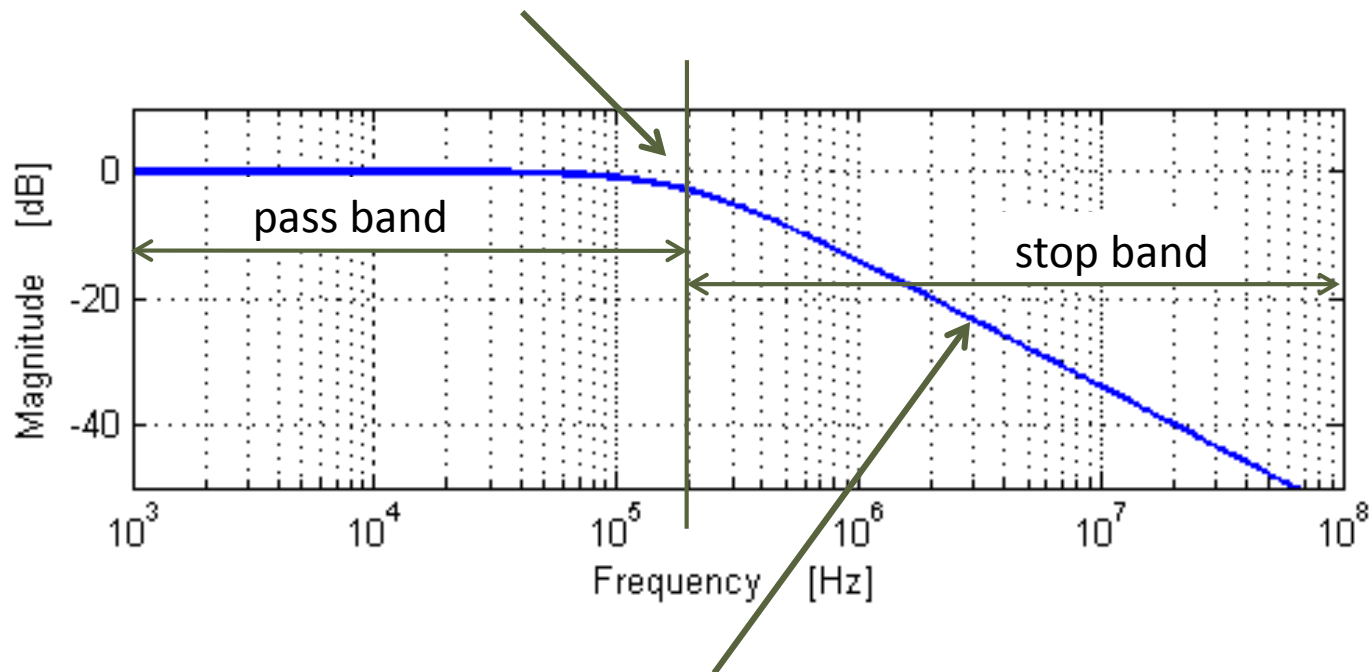
- Note the use of a linear gain scale here
  - Stop band gain of zero translates to  $-\infty$  dB
- Ideal filters often referred to as ***brick wall filters***

# Real Filters – Magnitude Response

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## Magnitude response for a real low pass filter:

Pass band edge is freq. at which gain is down by 3 dB – the **-3 dB frequency**.  
This is the filter's **bandwidth**.



**Roll-off rate** between pass band and stop band depends on the type of filter – particularly, the **order** of the filter.

# First-Order Passive Filters

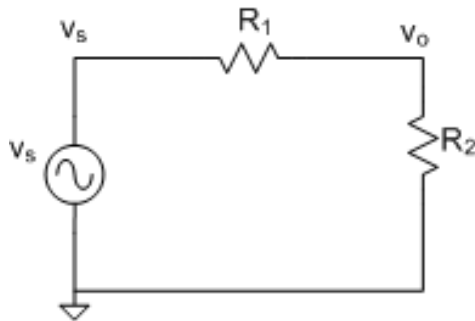
***First-order*** – only one energy-storage element

***Passive*** – contain only resistors and capacitors  
or inductors – no opamps or transistors

# Filters as Voltage Dividers

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- Already familiar with resistive voltage dividers:



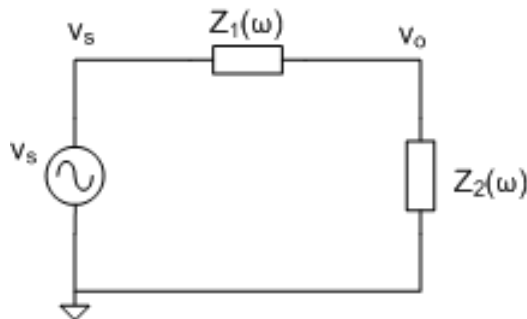
$$v_o = v_s \frac{R_2}{R_1 + R_2}$$

- Frequency response function:

$$H(\omega) = \frac{V_o}{V_s} = \frac{R_2}{R_1 + R_2}$$

- A real constant – independent of frequency
  - ▣ Same gain at all frequencies
  - ▣ No phase shift at any frequency

- 
- Now consider a circuit whose resistances have been replaced with impedances :



$$H(\omega) = \frac{V_o}{V_s} = \frac{Z_2}{Z_1 + Z_2}$$

- Frequency response is now a complex function of frequency
  - ▣ Gain and phase vary as a function of frequency
  - ▣ Basis for the design of first-order filters

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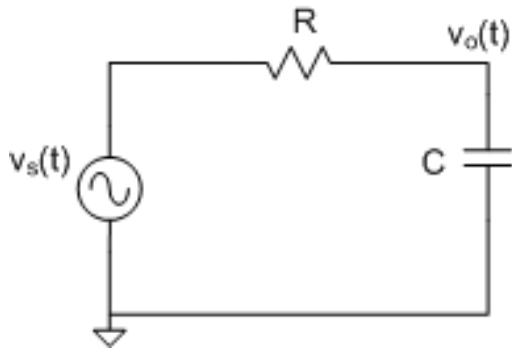
# RC Low Pass Filter

# RC Low Pass Filter

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- Now, let  $Z_1$  be resistive and  $Z_2$  be capacitive

- Frequency response:



$$H(\omega) = \frac{V_o}{V_s} = \frac{Z_2}{Z_1 + Z_2} = \frac{1/j\omega C}{R + 1/j\omega C}$$

$$H(\omega) = \frac{1}{1 + j\omega RC}$$

- Recall from ENGR 201 that the transient response of this same circuit is characterized by its time constant,  $\tau = RC$
- In the frequency domain, this is the **corner frequency** or **break frequency**

$$\omega_c = \frac{1}{\tau} = \frac{1}{RC}$$

and

$$f_c = \frac{1}{2\pi RC}$$

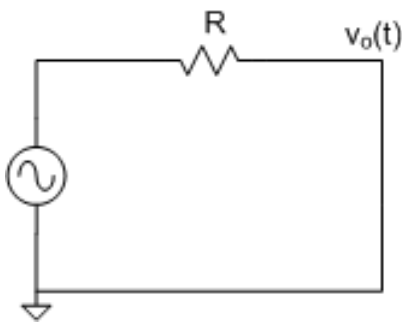
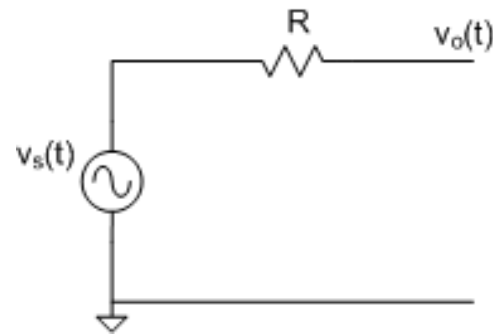
- The frequency at which gain is down by 3 dB
- The **-3 dB frequency**
- Frequency at which the magnitude of R and C impedances are equal

# RC Low Pass Filter

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- To gain insight into the behavior of this filter circuit, consider two limiting cases

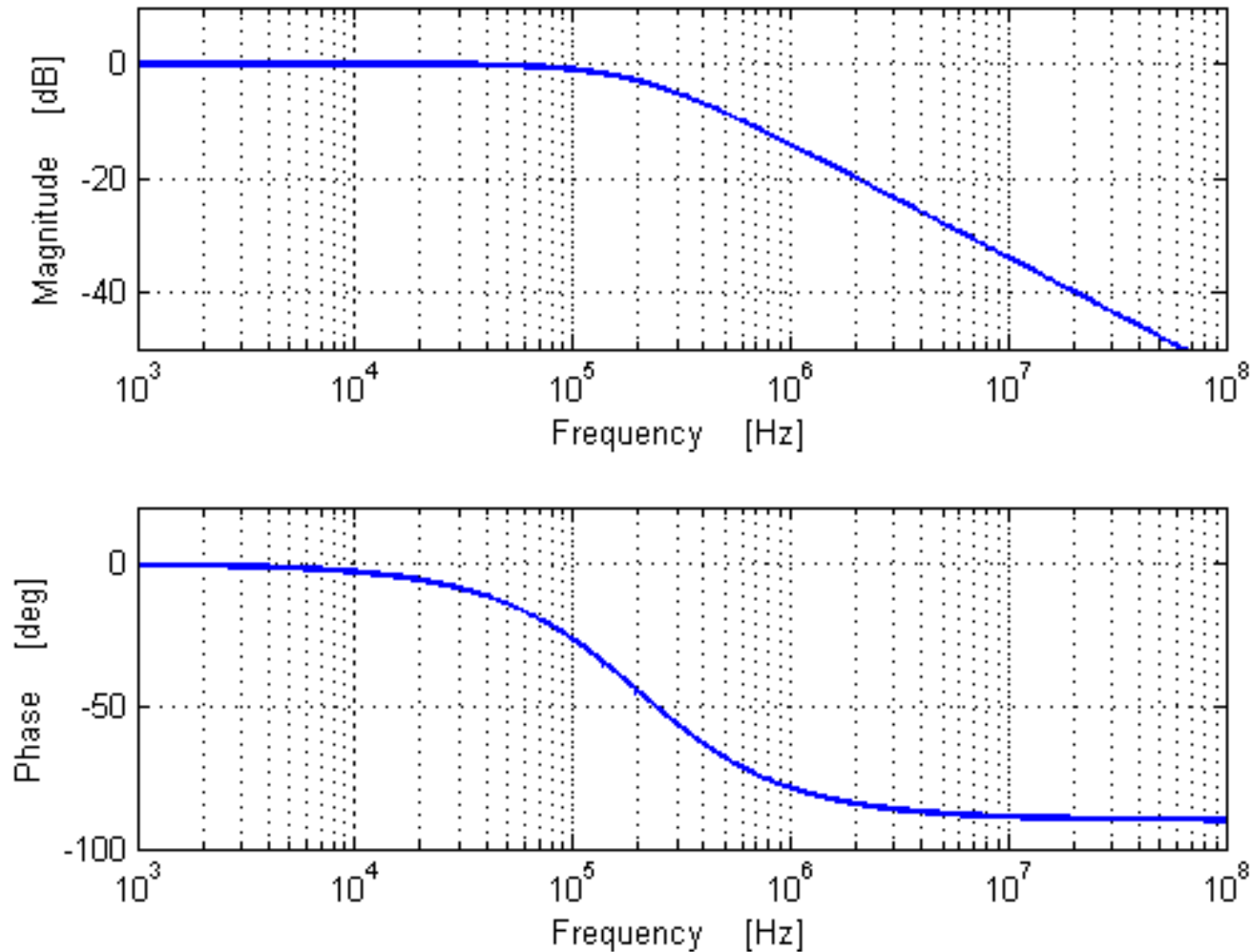
- As  $f \rightarrow 0$ ,
  - Capacitor  $\rightarrow$  open circuit
  - $i(t) \rightarrow 0$
  - $v_o \rightarrow v_s$
  - **Gain  $\rightarrow$  unity**



- As  $f \rightarrow \infty$ 
  - Capacitor  $\rightarrow$  short circuit
  - $v_o$  shorted to ground
  - **Gain  $\rightarrow$  zero**

# RC Low Pass Filter – Bode Plot

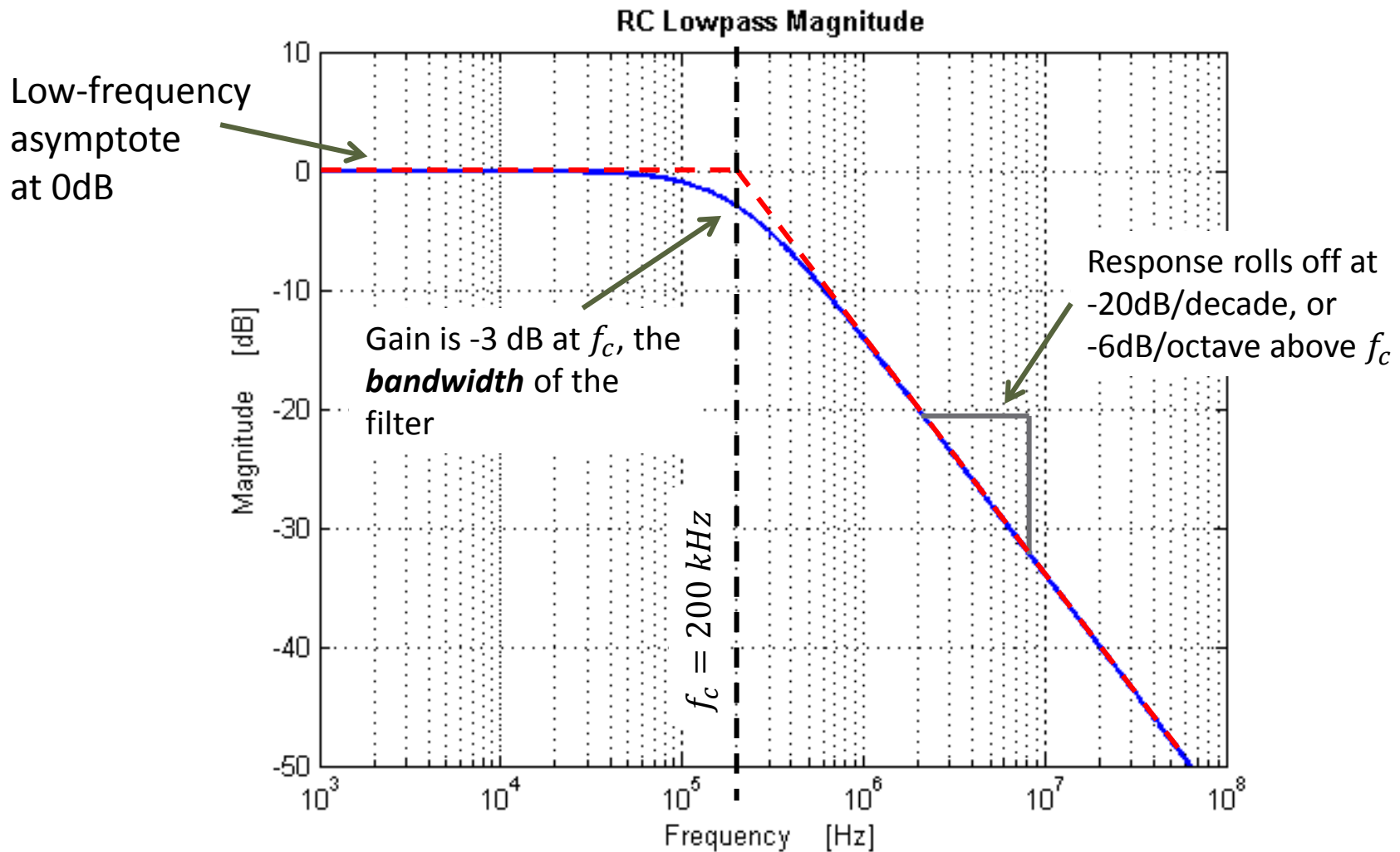
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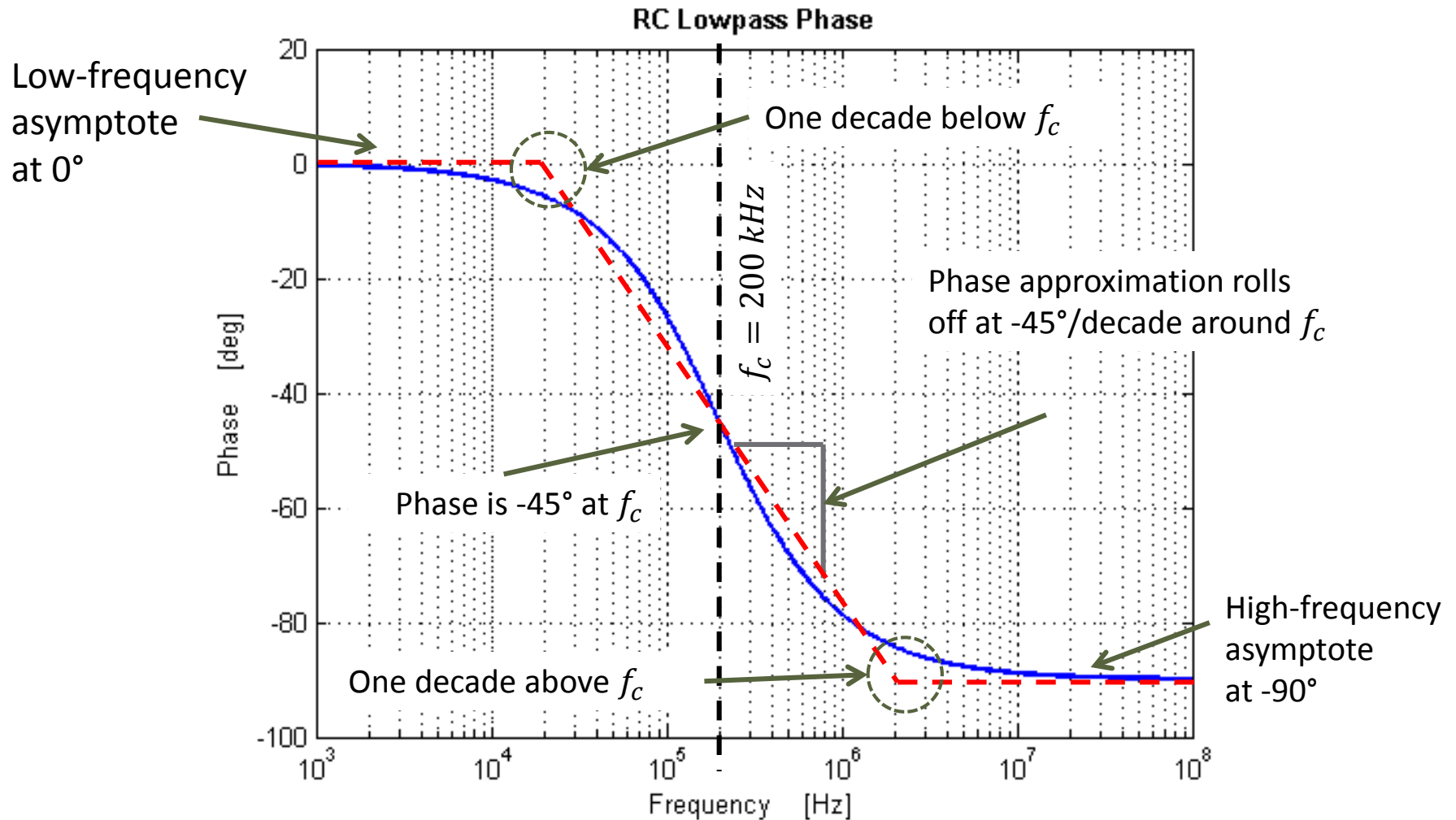
# RC Low Pass Filter – Magnitude Response

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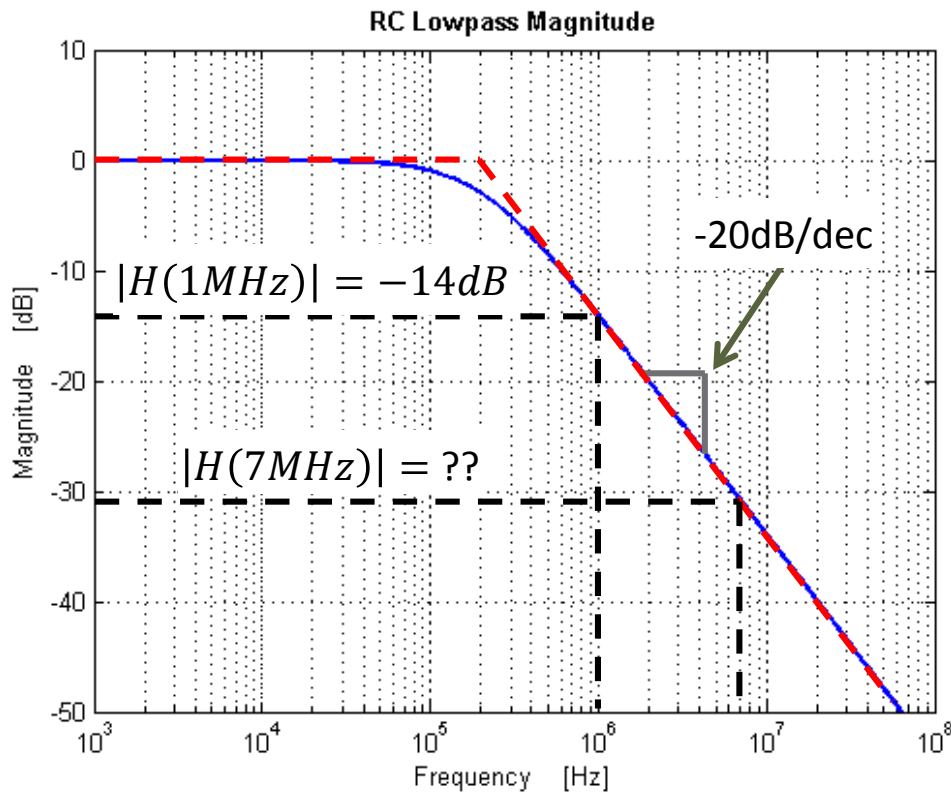
# RC Low Pass Filter – Phase Response

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# RC Low Pass Filter – Magnitude Response

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- Known slope can be used to relate gains at different frequencies

$$\text{Slope} \left[ \frac{dB}{dec} \right] = \frac{|H(f_2)|_{dB} - |H(f_1)|_{dB}}{\log_{10}(f_2) - \log_{10}(f_1)}$$

- For example:

$$-20 \frac{dB}{dec} = \frac{|H(7MHz)| - |H(1MHz)|_{dB}}{\log_{10}(7MHz) - \log_{10}(1MHz)}$$

$$-20 \frac{dB}{dec} = \frac{|H(7MHz)| - (-14dB)}{6.845 - 6}$$

$$|H(7MHz)| = -30.9dB$$

# RC LP Filter – Application Example

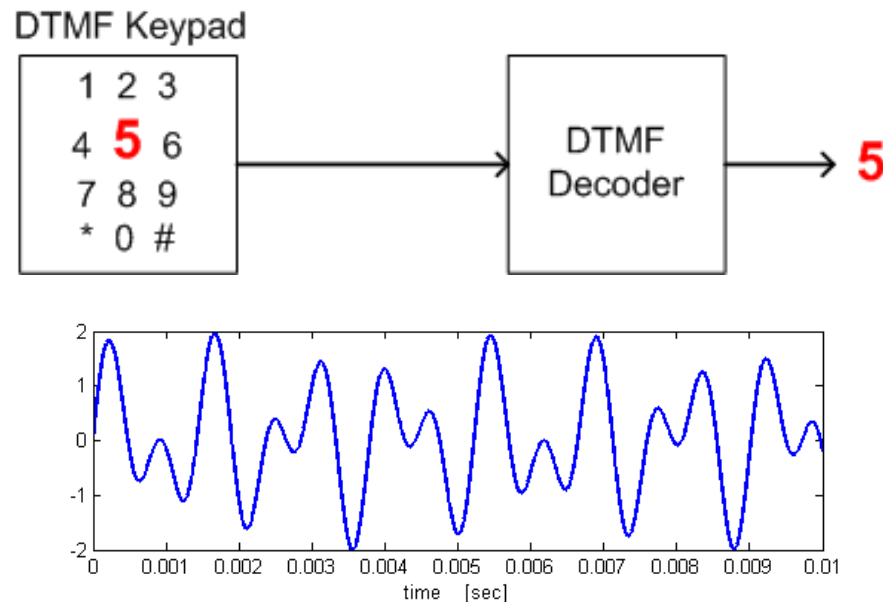
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- Simple first-order RC low pass filters provide a quick and easy way to remove noise from electrical signals
- 
- Consider for example a *dual-tone multi-frequency (DTMF)* signal
    - Touch-tone telephone signal (key **5** in this example)
    - Tone is the sum of two sinusoids (key 5 = 1336Hz and 770Hz)
    - Pressing the “5” key generates the DTMF signal
    - Noise on the DTMF signal makes decoding impossible
    - Filter noise to enabling decoding

# RC LP Filter – Application Example

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- Key number 5 is pressed
  - ▣ DTMF signal generated
    - Sum of 770 Hz and 1336 Hz sinusoids

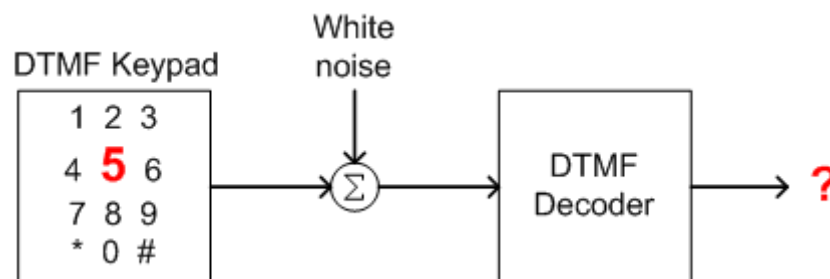


- ▣ Decoder at the receiving end decodes the DTMF signal and determines that a 5 was pressed

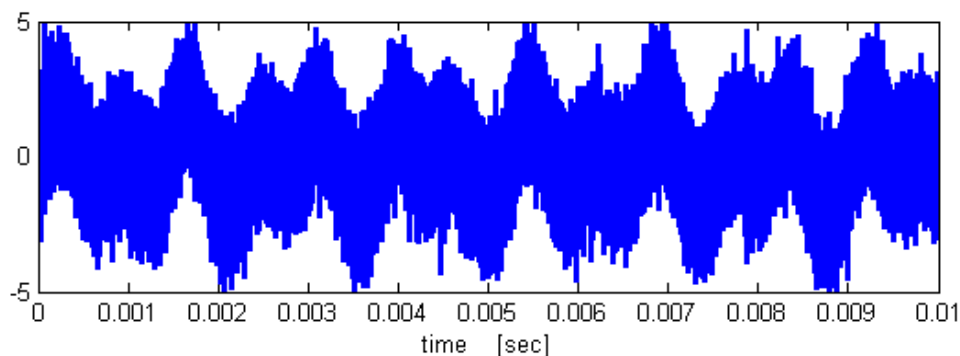
# RC LP Filter – Application Example

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- Consider a more realistic scenario
  - ▣ DTMF signal corrupted by a significant amount of noise



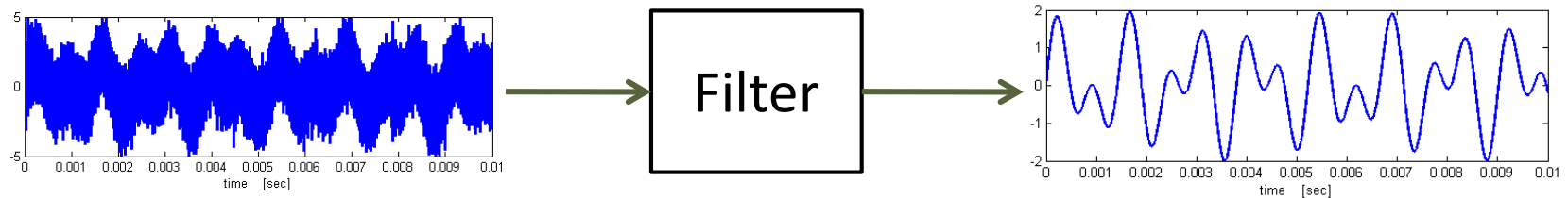
- ▣ The decoder is no longer able to determine that a 5 was pressed



# RC LP Filter – Application Example

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- The goal is to filter the received signal so that the decoder can accurately interpret the DTMF signal



- Designing the low pass filter
  - White noise
    - Flat frequency spectrum
    - Equal power at all frequencies
  - DTMF frequency range: 697 Hz – 1633 Hz
  - Want to attenuate as much noise as possible
  - Want to attenuate DTMF signals as little as possible
  - RC LPF with corner frequency at 10 kHz will limit DTMF-band attenuation to  $< 0.2$  dB

# RC LP Filter – Application Example

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## □ RC LPF design

- ▣ Need to select R and C to set the corner frequency

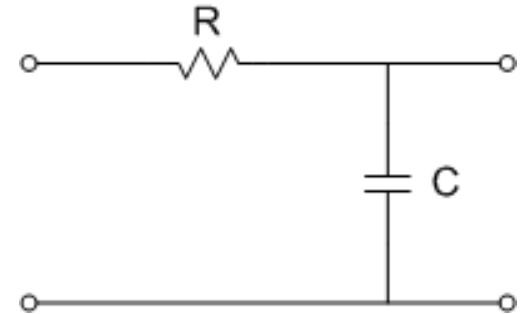
$$f_c = \frac{1}{2\pi RC} = 10 \text{ kHz}$$

- ▣ Say we have a  $0.1 \mu\text{F}$  capacitor available
- ▣ Solve for R

$$R = \frac{1}{2\pi f_c C}$$

$$R = \frac{1}{2\pi \cdot 10 \text{ kHz} \cdot 0.1 \mu\text{F}} = 159 \Omega$$

$$R = 159 \Omega, \quad C = 0.1 \mu\text{F}$$



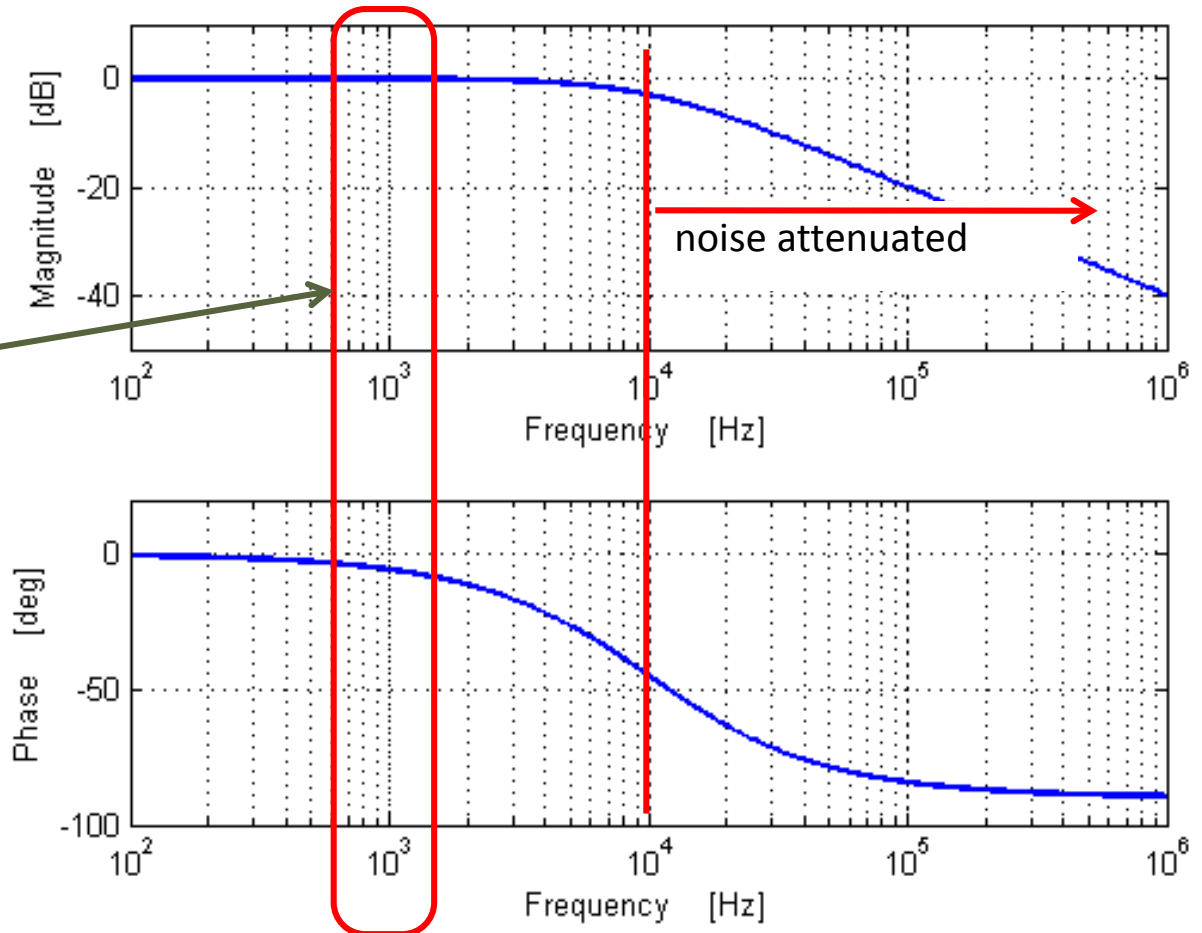


# RC LP Filter – Application Example

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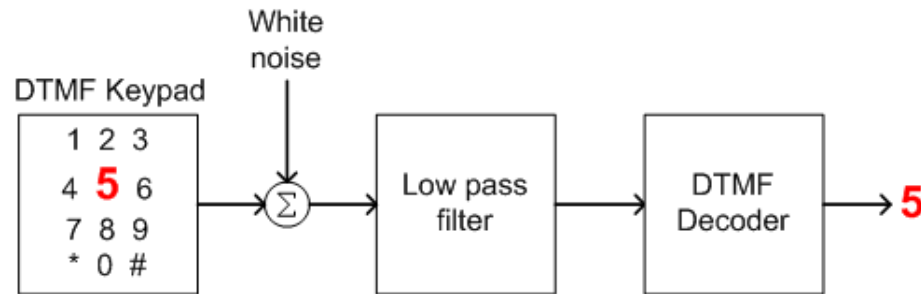
## Bode plot of the resulting filter:

DTMF signals lie in this range – passed through the filter with little attenuation

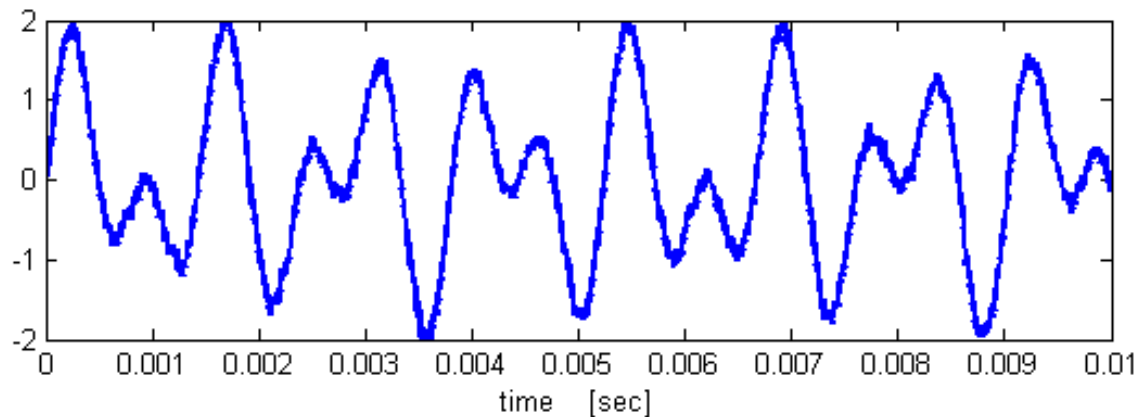


# RC LP Filter – Application Example

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- Filter allows DTMF signal to pass mostly unaltered
- Noise below 10 kHz is mostly passed through
- Noise above 10 kHz is attenuated, but not removed
- Received signal is not noiseless, but clean enough to be decoded

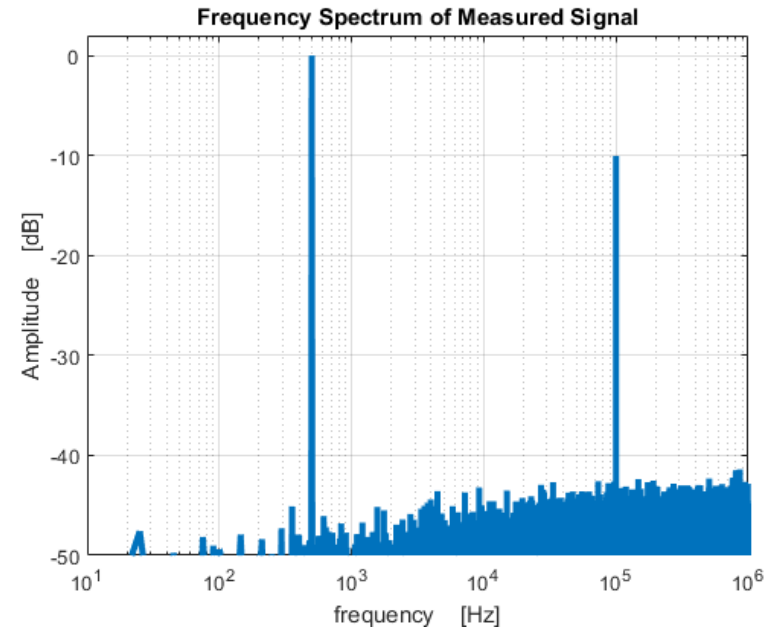


51

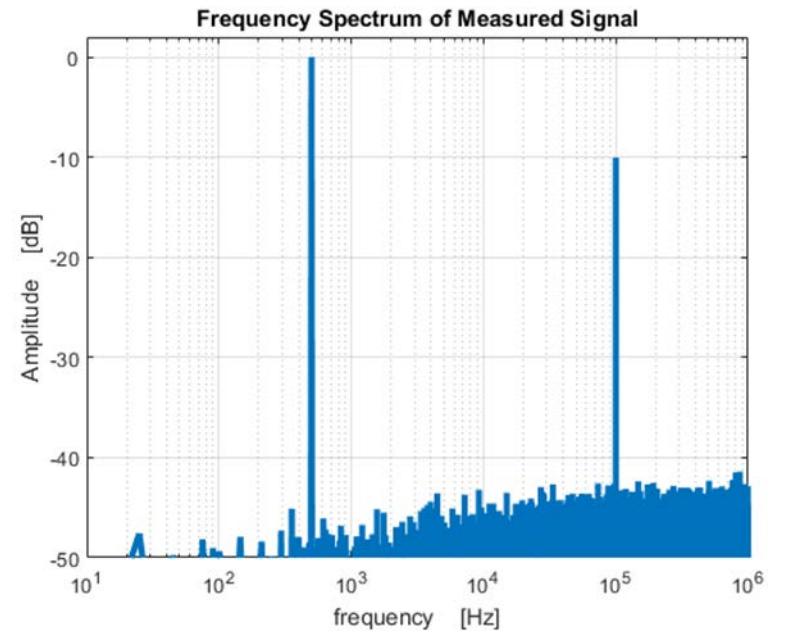
# Example Problems

Design a filter to pass the desired 500 Hz signal and to attenuate the unwanted 100 kHz by 40 dB.

What is the signal-to-noise ratio (SNR) at the output of the filter?







55

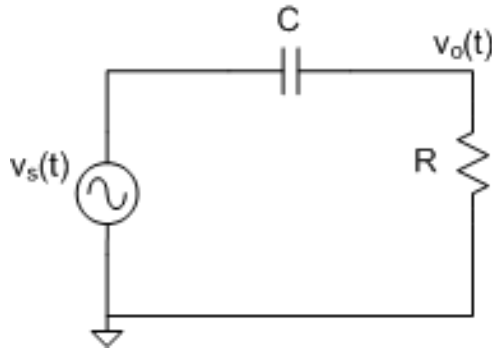
# RC High Pass Filter

# RC High Pass Filter

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- Now, swap the locations of the resistor and capacitor

- Frequency response:



$$H(\omega) = \frac{V_o}{V_s} = \frac{Z_2}{Z_1 + Z_2} = \frac{R}{R + 1/j\omega C}$$

$$H(\omega) = \frac{j\omega RC}{1 + j\omega RC}$$

- Corner frequency is the same as for the low pass filter

$$\omega_c = \frac{1}{\tau} = \frac{1}{RC}$$

and

$$f_c = \frac{1}{2\pi RC}$$

- The frequency at which gain is down by 3 dB
- Frequency at which the capacitor impedance magnitude is equal to the resistor impedance magnitude
- Now, gain is constant *above*  $f_c$  and rolls off *below*  $f_c$

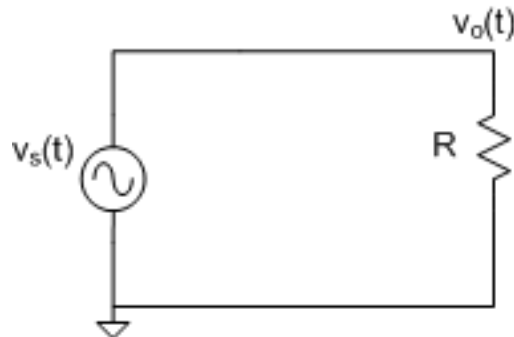
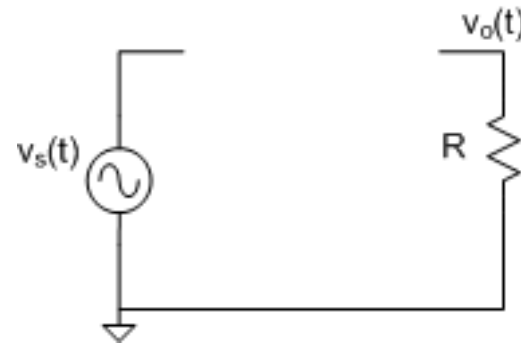


# RC High Pass Filter

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- To gain insight into the behavior of this filter circuit, consider two limiting cases

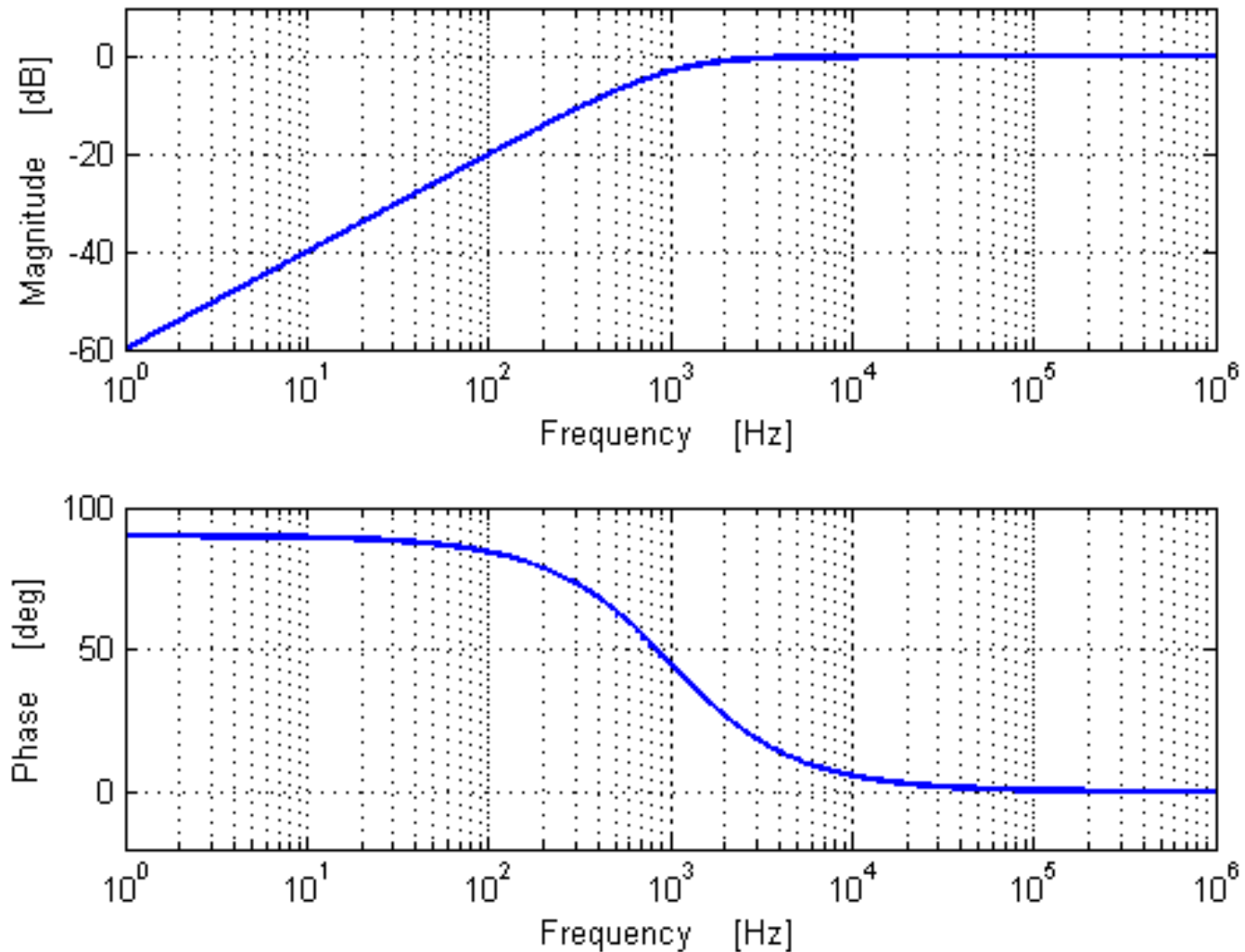
- As  $f \rightarrow 0$ ,
  - Capacitor  $\rightarrow$  open circuit
  - $i(t) \rightarrow 0$
  - $v_o \rightarrow 0$
  - **Gain  $\rightarrow$  zero**



- As  $f \rightarrow \infty$ 
  - Capacitor  $\rightarrow$  short circuit
  - $v_o$  shorted to  $v_s$
  - **Gain  $\rightarrow$  unity**

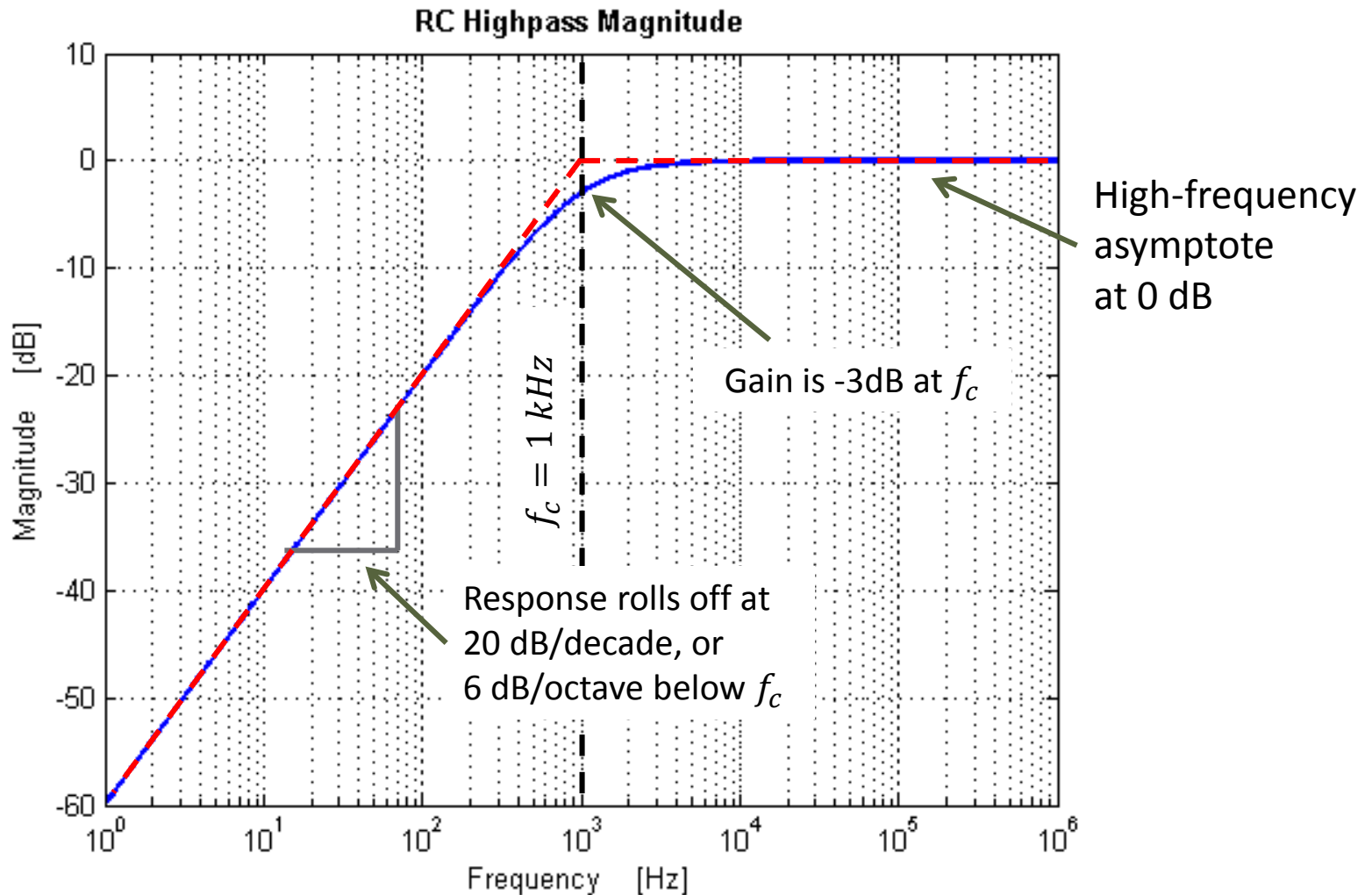
# RC High Pass Filter – Bode Plot

58



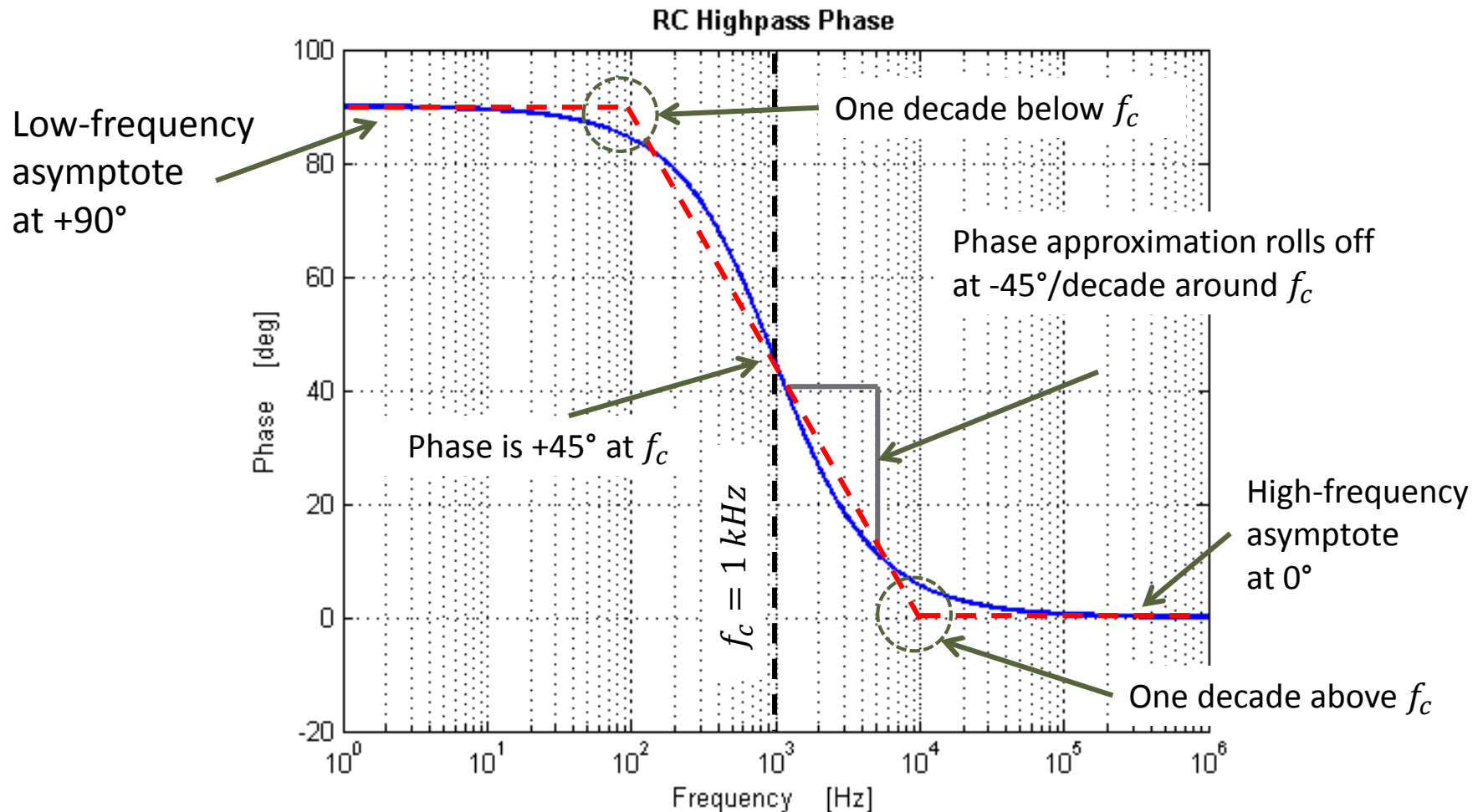
# RC High Pass Filter – Magnitude Response

59



# RC High Pass Filter – Phase Response

60



# RC HP Filter – Application Example

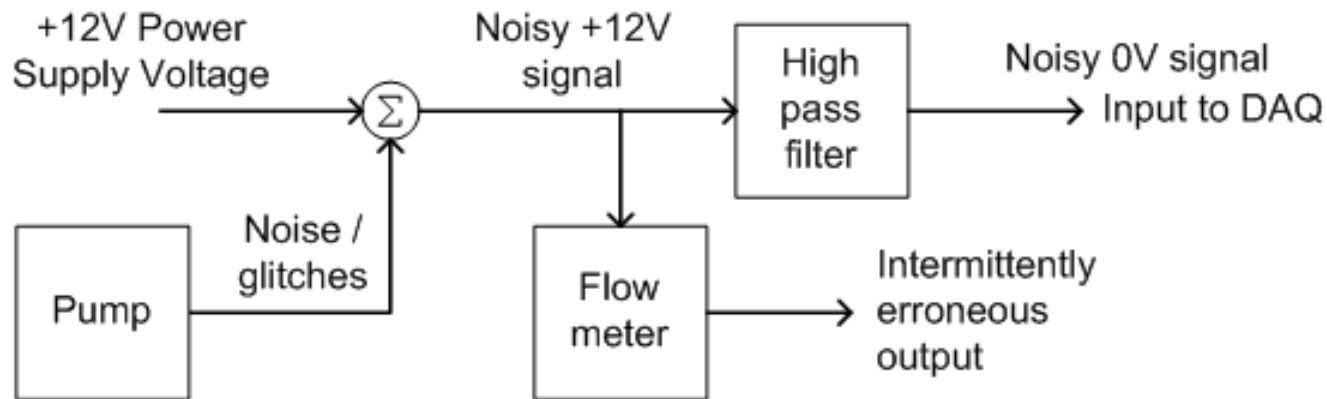
61

- High pass filters are useful for removing low-frequency content, including DC, from electrical signals.
- 
- For example, consider the following scenario:
    - Instrumented a flow loop in the lab
      - Pumps, temperature sensors, pressure sensors, and flow meters
    - Flow meter output seems to be erroneous every  $\sim 1$  msec
    - Suspected cause: coupled through the +12V power supply from one of the pumps
    - Want to measure the flow meter's +12V power supply with a channel on our data acquisition system (DAQ)
      - Dynamic range of DAQ input:  $\pm 5$  V
    - Use a high-pass filter to remove the +12V DC component from the power supply voltage

# RC HP Filter – Application Example

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- Want to a +12 V supply with a  $\pm 5$  V DAQ input
- High pass filter will remove the DC component of the supply voltage

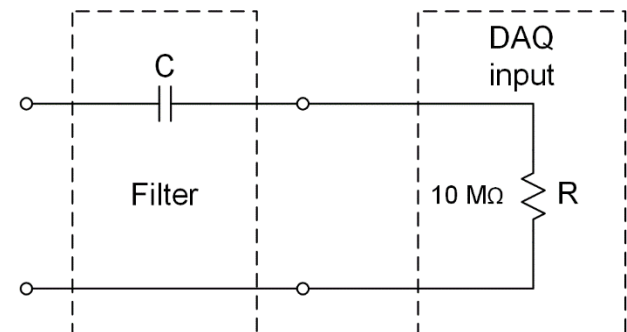
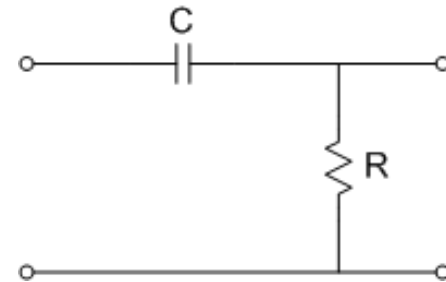


- High pass filter used to remove DC signal components
- Couples only AC signal components to the DAQ input
  - AC coupling
  - Similar to the AC coupling setting on the scopes in the lab

# RC HP Filter – Application Example

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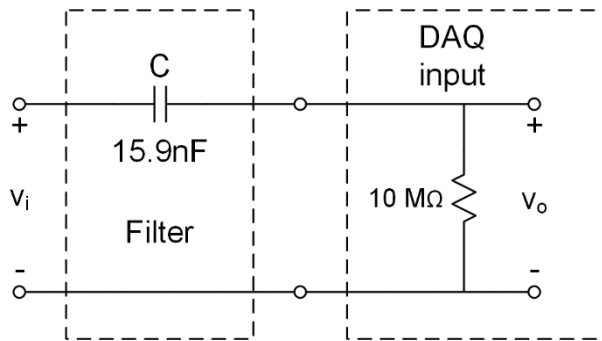
- High pass filter design
  - Want to remove DC
    - Low corner frequency
  - High RC time constant
    - Large R and C
  - Arbitrarily set  $f_c = 10 \text{ Hz}$
- DAQ system
  - Datasheet says  $R_{in} = 10 \text{ M}\Omega$ 
    - Let  $R_{in}$  be the filter resistance
- Calculate C to get desired  $f_c$ 
$$C = \frac{1}{2\pi f_c R} = \frac{1}{2\pi \cdot 10\text{Hz} \cdot 10\text{M}\Omega}$$
$$C = 15.9 \text{ nF}$$
  - Or anything in that neighborhood
  - Not critical – just want to block DC



# RC HP Filter – Application Example

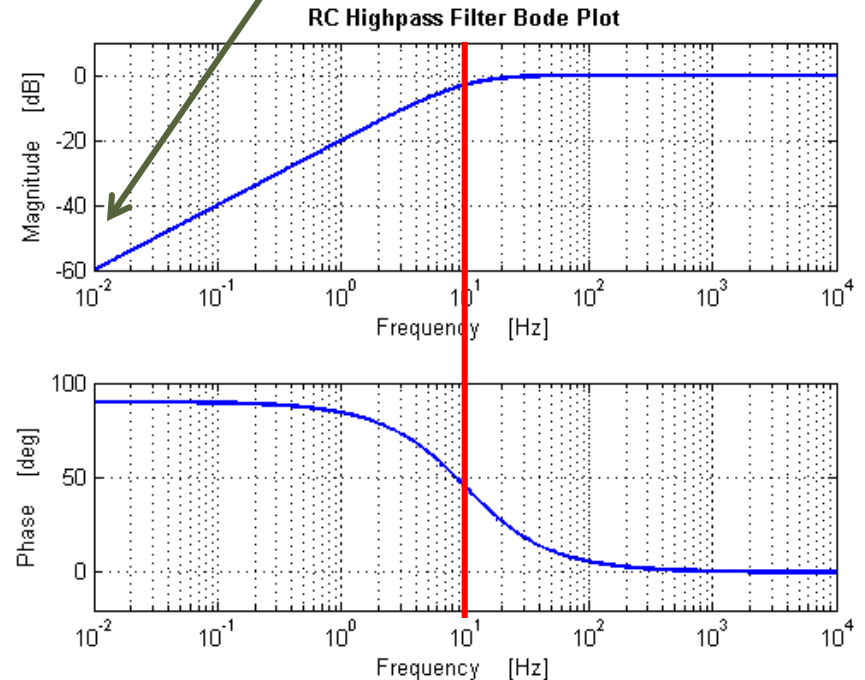
64

## RC high pass filter:



## High pass filter Bode plot:

The +12V DC component of the power supply voltage is completely removed.



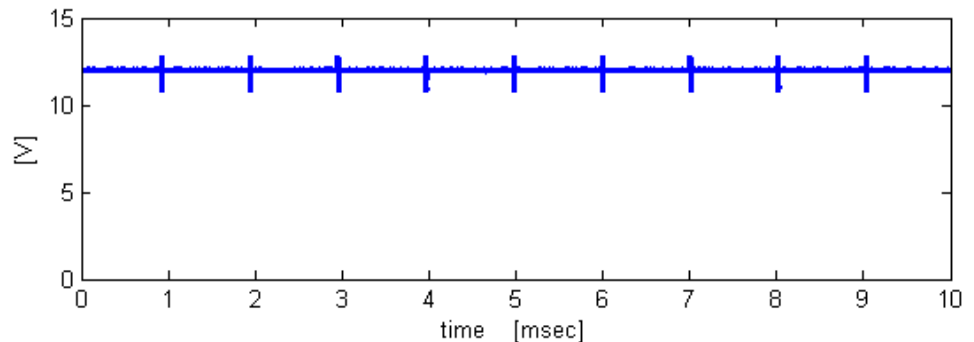


# RC HP Filter – Application Example

65

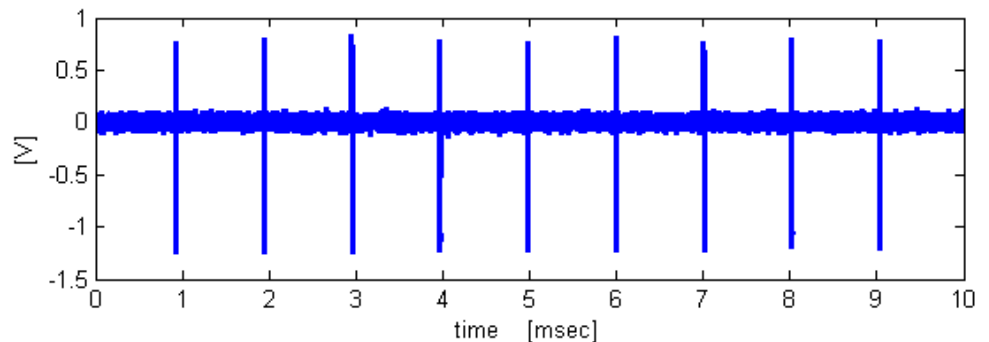
## The noisy +12V power supply at the malfunctioning flow meter:

- DC value of signal is +12 V
- Outside  $\pm 5$  V DAQ input dynamic range



## High pass filter output – AC coupled power supply voltage:

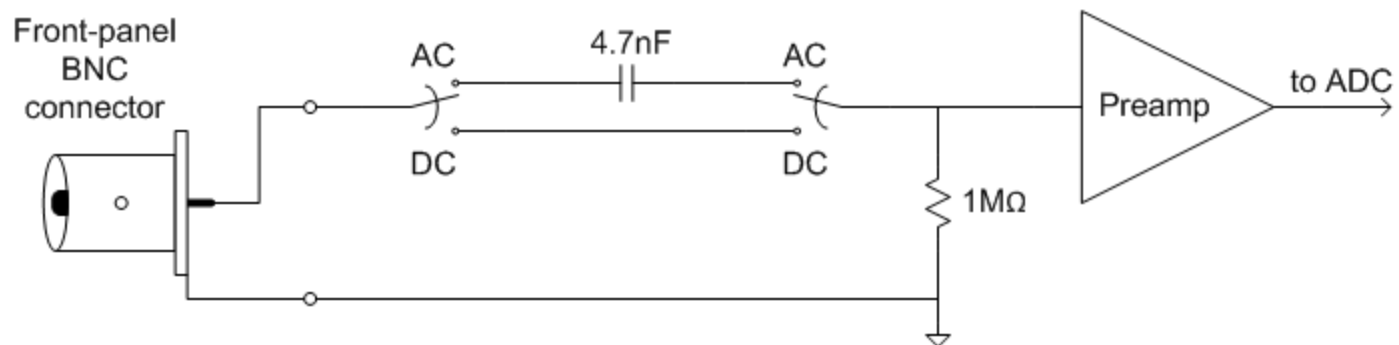
- DC value of signal is now 0 V
- Within  $\pm 5$  V DAQ input range
- Glitches clearly measured with the DAQ



# Oscilloscopes – AC Coupling

66

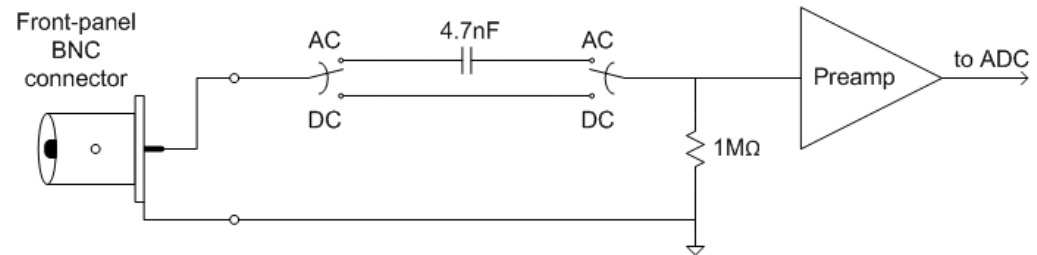
- Scope inputs allow you to select between DC and AC coupling
  - ▣ Usually under the *channel* menu
  - ▣ **DC coupling**: input signal is terminated in  $1\text{M}\Omega$  and connected directly to the preamp and ADC in the scope
  - ▣ **AC coupling**: input signal is switched through a capacitor that forms a high pass filter with the  $1\text{M}\Omega$  input resistor
    - $f_c \approx 3.5\text{ Hz}$  – removes DC
    - Useful for looking at power supply ripple, etc.



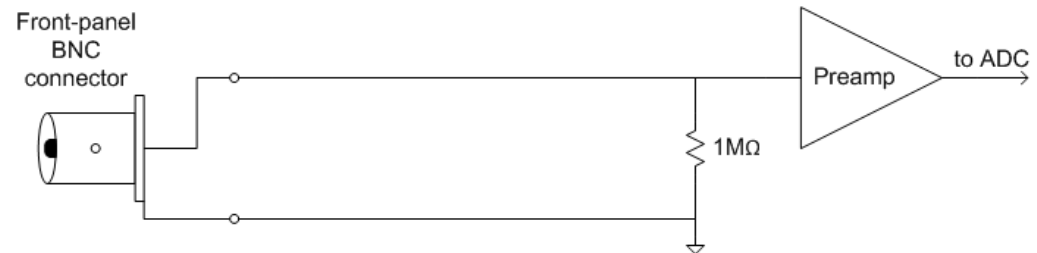
# Oscilloscopes – AC Coupling

67

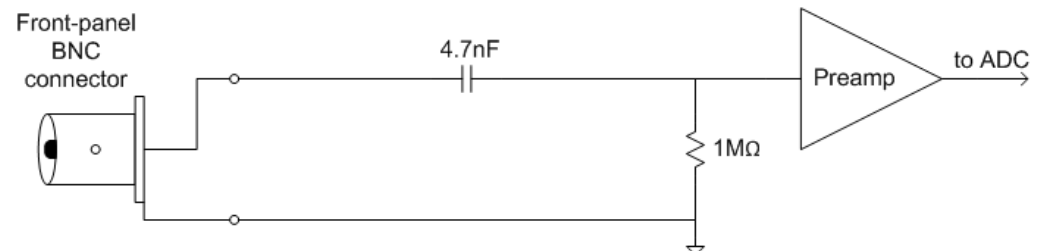
## High-impedance scope front-end:



## Configured for DC coupling:



## Configured for AC coupling:



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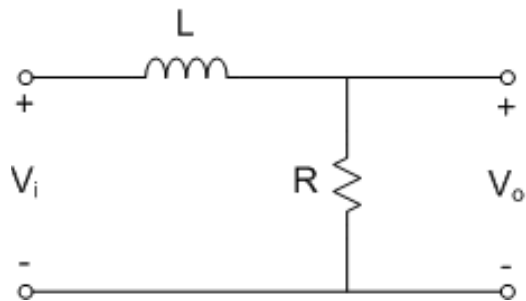
# RL Filters

# First-order RL filters

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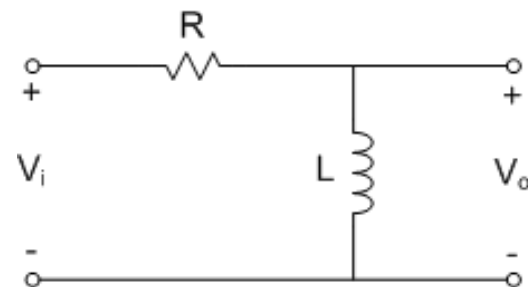
- Can also use **inductors** to make **RL** low pass and high pass filters
- Capacitors are usually preferable for simple first-order filters
  - ▣ Smaller
  - ▣ Cheaper
  - ▣ Draw no DC current

## RL low pass filter:



Corner frequency:  $f_c = \frac{R}{2\pi L}$

## RL high pass filter:

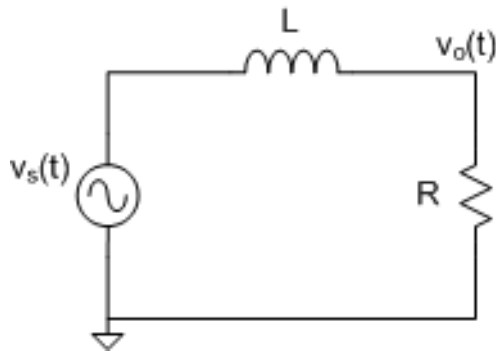


Corner frequency:  $f_c = \frac{R}{2\pi L}$

# RL Low Pass Filter

70

## □ RL low pass filter



## □ Frequency response:

$$H(\omega) = \frac{V_o}{V_s} = \frac{Z_2}{Z_1 + Z_2} = \frac{R}{R + j\omega L}$$

$$H(\omega) = \frac{R}{R + j\omega L}$$

## □ Corner frequency is one over the time constant

$$\omega_c = \frac{1}{\tau} = \frac{R}{L}$$

and

$$f_c = \frac{R}{2\pi L}$$

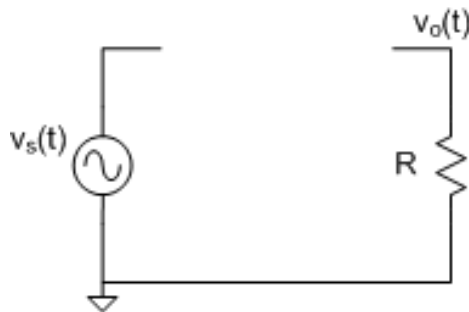
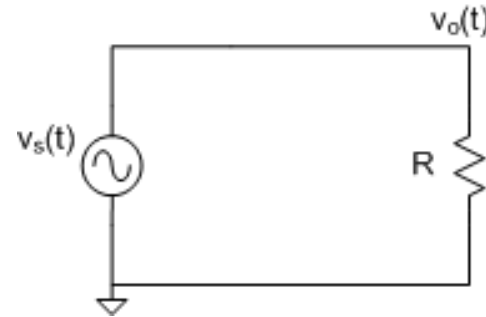
- The frequency at which gain is down by 3 dB
- Frequency at which the inductor impedance magnitude is equal to the resistor impedance magnitude
- Bode plot identical to that of the RC low pass filter
  - As it is for all first-order low pass systems

# RL Low Pass Filter

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- Again consider the filter's behavior for two limiting cases

- As  $f \rightarrow 0$ ,
  - Inductor  $\rightarrow$  short circuit
  - $v_o$  shorted to  $v_s$
  - **Gain  $\rightarrow$  unity**

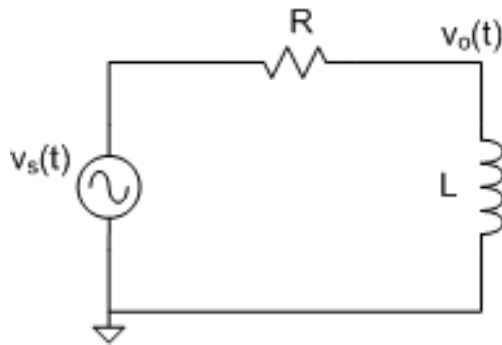


- As  $f \rightarrow \infty$ 
  - Inductor  $\rightarrow$  open circuit
  - $i(t) \rightarrow 0$
  - $v_o \rightarrow 0$
  - **Gain  $\rightarrow$  zero**

# RL High Pass Filter

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- Now, swap the locations of the resistor and inductor



- Frequency response:

$$H(\omega) = \frac{V_o}{V_s} = \frac{Z_2}{Z_1 + Z_2} = \frac{j\omega L}{R + j\omega L}$$

$$H(\omega) = \frac{j\omega L}{R + j\omega L}$$

- Corner frequency is the same as for the low pass filter

$$\omega_c = \frac{1}{\tau} = \frac{R}{L}$$

and

$$f_c = \frac{R}{2\pi L}$$

- Bode plot is identical to that of the RC high pass filter
- Gain is constant *above*  $f_c$  and rolls off *below*  $f_c$



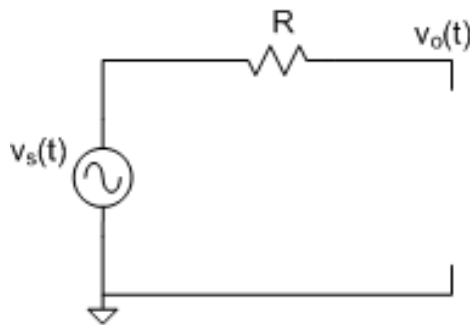
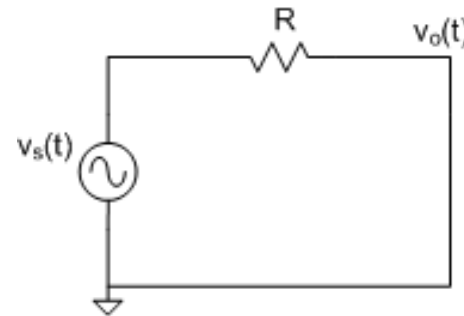
# RL High Pass Filter

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- Again, consider the two limiting frequency cases

- As  $f \rightarrow 0$ ,

- Inductor  $\rightarrow$  short circuit
- $v_o$  shorted to ground
- **Gain  $\rightarrow$  zero**



- As  $f \rightarrow \infty$

- Inductor  $\rightarrow$  open circuit
- $i(t) \rightarrow 0$
- $v_o \rightarrow v_s$
- **Gain  $\rightarrow$  unity**

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# Audio Filter Demo

# Analog Discovery Instrument

75

- 2-chan. Scope
  - 14-bit, 100MSa/s
  - 5MHz bandwidth
- 2-chan. function generator
  - 14-bit, 100MSa/s
  - 5MHz bandwidth
- 2-chan. spectrum analyzer
- Network analyzer
- Voltmeter
- $\pm 5V$  power supplies
- 16-chan. logic analyzer
- 16-chan. digital pattern generator
- USB connectivity



# Analog Discovery – Audio Demo

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- Demo board plugs in to Analog Discovery module
- Summation of multiple tones
- Optional filtering of audio signal
- 3.5 mm audio output jack



# Analog Discovery – Audio Demo

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