

SECTION 7: THREE-PHASE CIRCUIT FUNDAMENTALS

ENGR 202 – Electrical Fundamentals II

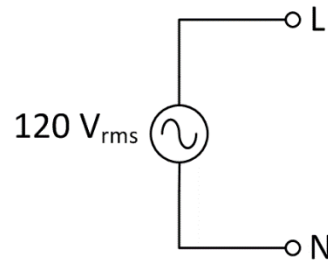
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Balanced Three-Phase Networks

Balanced Three-Phase Networks

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- We are accustomed to **single-phase** power in our homes and offices
 - ▣ A single **line** voltage referenced to a **neutral**



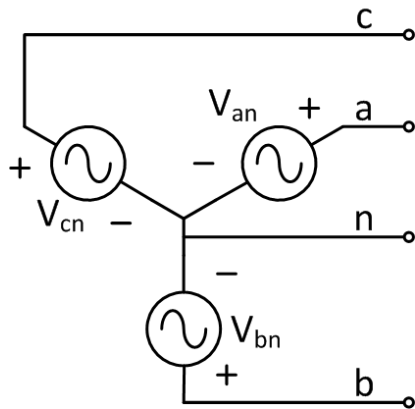
- Electrical power is generated, transmitted, and largely consumed (by industrial customers) as **three-phase power**
 - ▣ Three individual line voltages and (possibly) a neutral
 - ▣ Line voltages all differ in phase by $\pm 120^\circ$

Δ - and Y-Connected Networks

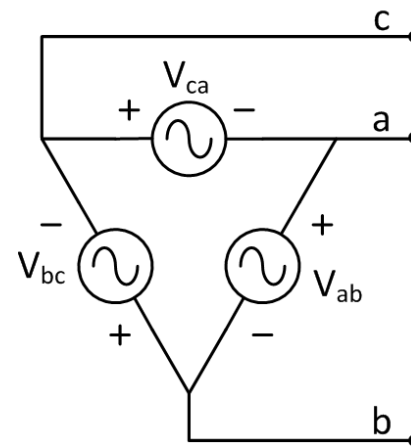
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- Two possible three-phase configurations
 - ▣ Applies to both *sources* and *loads*

Y-Connected Source



Δ -Connected Source

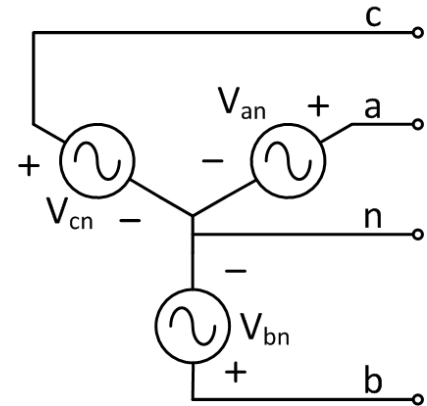


- Y-connected network has a neutral node
- Δ -connected network has no neutral

Line-to-Neutral Voltages

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- In the Y network, voltages V_{an} , V_{bn} , and V_{cn} are **line-to-neutral voltages**
- A three-phase source is **balanced** if
 - ▣ Line-to-neutral voltages have equal magnitudes
 - ▣ Line-to-neutral voltages are each 120° out of phase with one another
- A three-phase network is balanced if
 - ▣ Sources are balanced
 - ▣ The impedances connected to each phase are equal



Line-to-Neutral Voltages

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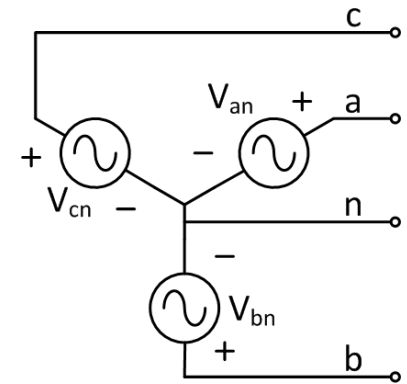
- The line-to-neutral voltages are

$$V_{an} = V_{LN} \angle 0^\circ$$

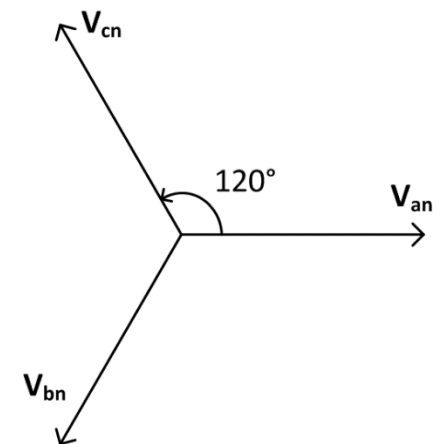
$$V_{bn} = V_{LN} \angle -120^\circ$$

$$V_{cn} = V_{LN} \angle -240^\circ = V_{LN} \angle +120^\circ$$

- This is a **positive-sequence** or **abc-sequence** source
 - V_{an} leads V_{bn} , which leads V_{cn}
- Can also have a **negative-** or **acb-sequence** source
 - V_{an} leads V_{cn} , which leads V_{bn}
- We'll always assume **positive-sequence** sources



Positive-Sequence Phasor Diagram:



Line-to-Line Voltages

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- The voltages between the three phases are **line-to-line voltages**
- Apply KVL to relate line-to-line voltages to line-to-neutral voltages

$$V_{ab} - V_{an} + V_{bn} = 0$$

$$V_{ab} = V_{an} - V_{bn}$$

- We know that

$$V_{an} = V_{LN} \angle 0^\circ$$

and

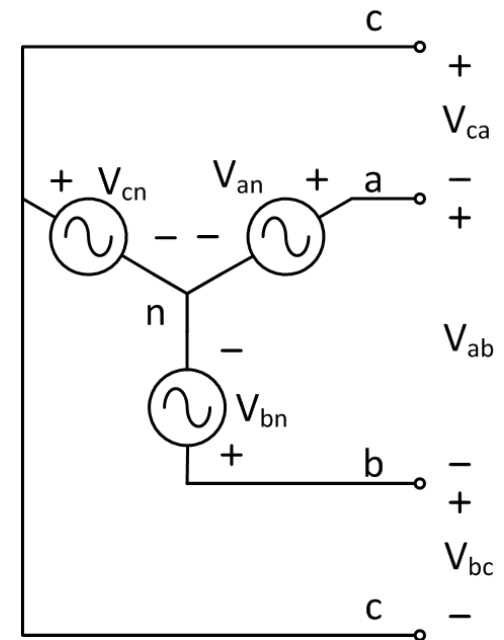
$$V_{bn} = V_{LN} \angle -120^\circ$$

so

$$V_{ab} = V_{LN} \angle 0^\circ - V_{LN} \angle -120^\circ = V_{LN} (1 \angle 0^\circ - 1 \angle -120^\circ)$$

$$V_{ab} = V_{LN} \left[1 - \left(-\frac{1}{2} - j\frac{\sqrt{3}}{2} \right) \right] = V_{LN} \left[\frac{3}{2} + j\frac{\sqrt{3}}{2} \right]$$

$$V_{ab} = \sqrt{3} V_{LN} \angle 30^\circ$$



Line-to-Line Voltages

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- Again applying KVL, we can find V_{bc}

$$V_{bc} = V_{bn} - V_{cn}$$

$$V_{bc} = V_{LN} \angle -120^\circ - V_{LN} \angle 120^\circ$$

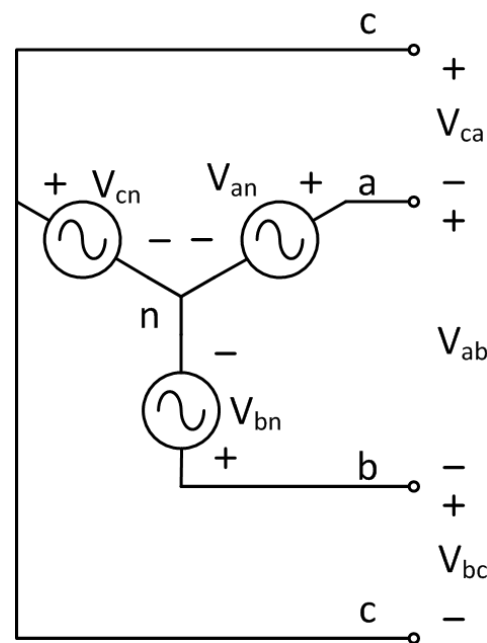
$$V_{bc} = V_{LN} \left[\left(-\frac{1}{2} - j\frac{\sqrt{3}}{2} \right) - \left(-\frac{1}{2} + j\frac{\sqrt{3}}{2} \right) \right]$$

$$V_{bc} = V_{LN} (-j\sqrt{3})$$

$$V_{bc} = \sqrt{3}V_{LN} \angle -90^\circ$$

- Similarly,

$$V_{ca} = \sqrt{3}V_{LN} \angle 150^\circ$$



Line-to-Line Voltages

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- The line-to-line voltages, with V_{an} as the reference:

$$V_{ab} = \sqrt{3}V_{LN} \angle 30^\circ$$

$$V_{bc} = \sqrt{3}V_{LN} \angle -90^\circ$$

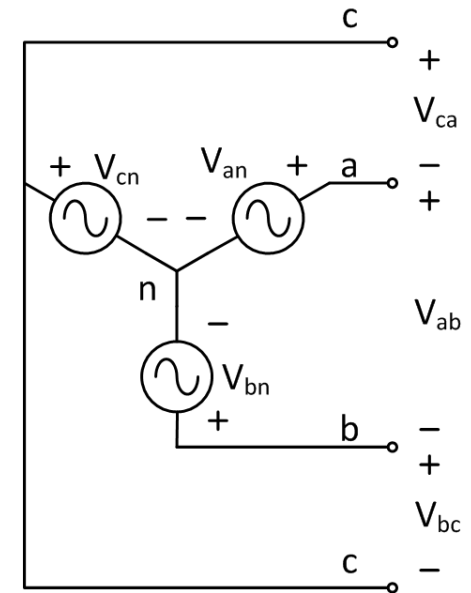
$$V_{ca} = \sqrt{3}V_{LN} \angle 150^\circ$$

- Line-to-line voltages are $\sqrt{3}$ times the line-to-neutral voltage
- Can also express in terms of individual line-to-neutral voltages:

$$V_{ab} = \sqrt{3}V_{an} \angle 30^\circ$$

$$V_{bc} = \sqrt{3}V_{bn} \angle 30^\circ$$

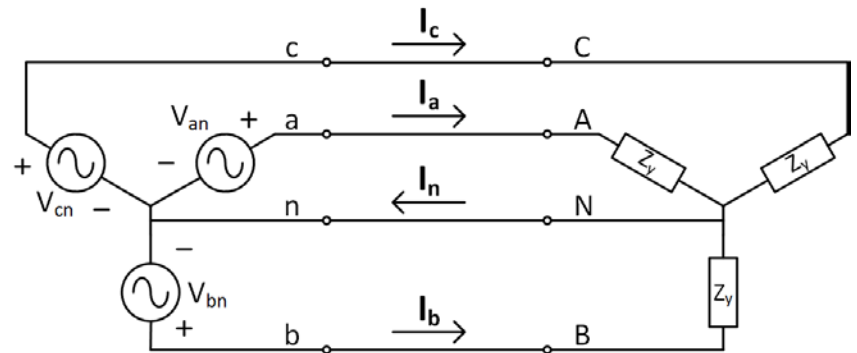
$$V_{ca} = \sqrt{3}V_{cn} \angle 30^\circ$$



Line Currents in Balanced 3 ϕ Networks

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- We can use the line-to-neutral voltages to determine the line currents
 - ▣ Y-connected source and load
 - ▣ Balanced load – all impedances are equal: Z_Y



$$\begin{aligned} I_a &= \frac{V_{AN}}{Z_Y} = \frac{V_{LN} \angle 0^\circ}{Z_Y} \\ I_b &= \frac{V_{BN}}{Z_Y} = \frac{V_{LN} \angle -120^\circ}{Z_Y} \\ I_c &= \frac{V_{CN}}{Z_Y} = \frac{V_{LN} \angle +120^\circ}{Z_Y} \end{aligned}$$

- Line currents are balanced as long as the source and load are balanced

Neutral Current in Balanced 3 ϕ Networks

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- Apply KCL to determine the neutral current

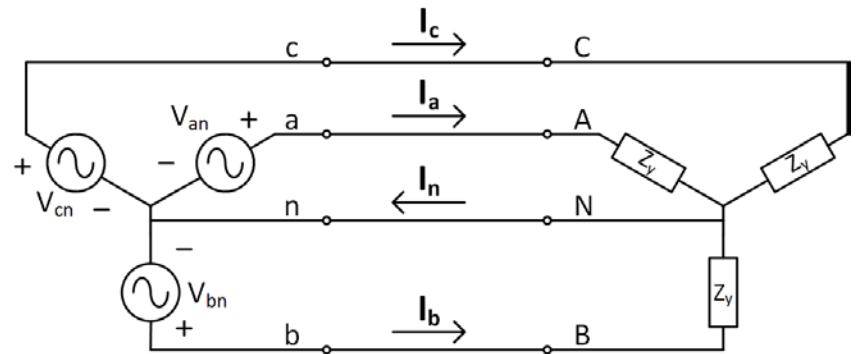
$$I_n = I_a + I_b + I_c$$

$$I_n = \frac{V_{LN}}{Z_Y} [1\angle 0^\circ + 1\angle -120^\circ + 1\angle 120^\circ]$$

$$I_n = \frac{V_{LN}}{Z_Y} \left[1 + \left(-\frac{1}{2} - j\frac{\sqrt{3}}{2} \right) + \left(-\frac{1}{2} + j\frac{\sqrt{3}}{2} \right) \right]$$

$$I_n = 0$$

- The neutral conductor carries no current in a balanced three-phase network



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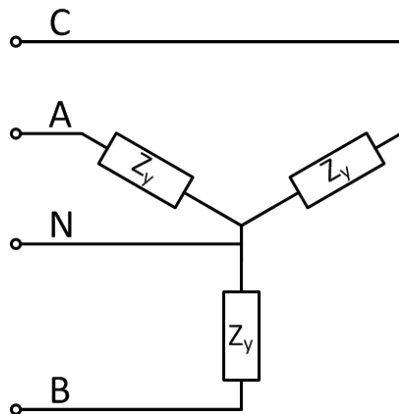
Delta- & Wye-Connected Networks

Three-Phase Network Configurations

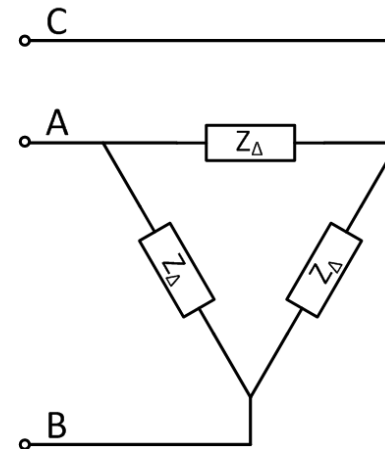
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- As for sources, three-phase loads can also be connected in two different configurations

Y-Connected Load



Δ -Connected Load

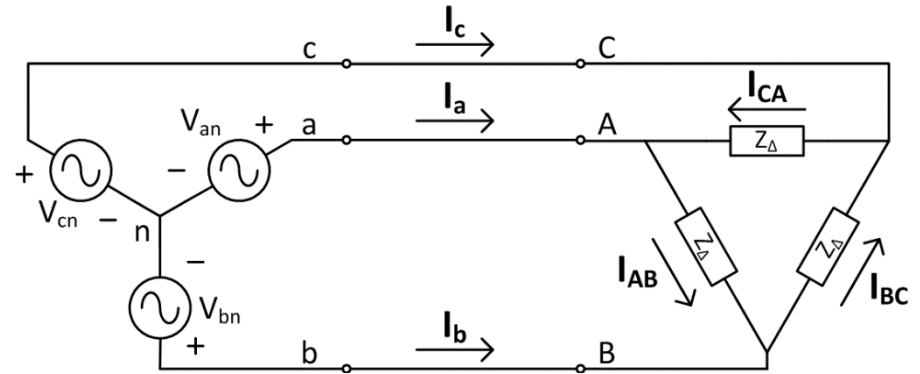


- The Y load has a neutral connection, but the Δ load does not
- Currents in a Y-connected load are the line currents we just determined
- Next, we'll look at currents in a Δ -connected load

Balanced Δ -Connected Loads

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- We can use line-to-line voltages to determine the currents in Δ -connected loads



$$I_{AB} = \frac{V_{AB}}{Z_{\Delta}} = \frac{\sqrt{3}V_{AN}\angle 30^{\circ}}{Z_{\Delta}} = \frac{\sqrt{3}V_{LN}\angle 30^{\circ}}{Z_{\Delta}}$$

$$I_{BC} = \frac{V_{BC}}{Z_{\Delta}} = \frac{\sqrt{3}V_{BN}\angle 30^{\circ}}{Z_{\Delta}} = \frac{\sqrt{3}V_{LN}\angle -90^{\circ}}{Z_{\Delta}}$$

$$I_{CA} = \frac{V_{CA}}{Z_{\Delta}} = \frac{\sqrt{3}V_{CN}\angle 30^{\circ}}{Z_{\Delta}} = \frac{\sqrt{3}V_{LN}\angle 150^{\circ}}{Z_{\Delta}}$$

Balanced Δ -Connected Loads

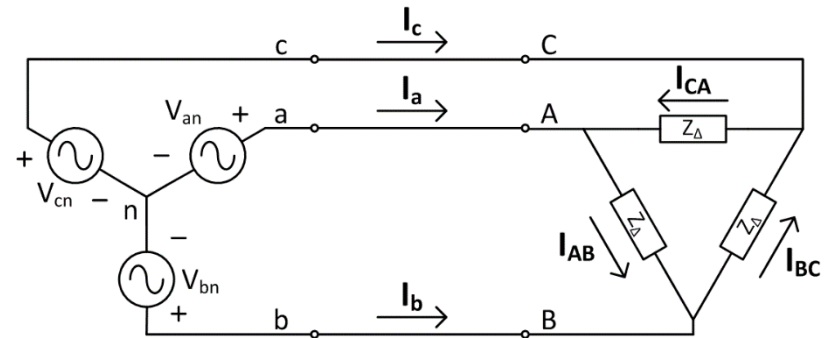
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- Applying KCL, we can determine the line currents

$$I_a = I_{AB} - I_{CA}$$

$$I_a = \frac{\sqrt{3}V_{LN}}{Z_{\Delta}} [1\angle 30^\circ - 1\angle 150^\circ]$$

$$I_a = \frac{\sqrt{3}V_{LN}}{Z_{\Delta}} \left[\left(\frac{\sqrt{3}}{2} + j\frac{1}{2} \right) - \left(-\frac{\sqrt{3}}{2} + j\frac{1}{2} \right) \right] = \frac{\sqrt{3}V_{LN}}{Z_{\Delta}} [\sqrt{3}] = \frac{3V_{LN}}{Z_{\Delta}}$$



- The other line currents can be found similarly:

$$I_a = \frac{3V_{LN}\angle 0^\circ}{Z_{\Delta}} = \sqrt{3}I_{AB}\angle -30^\circ$$

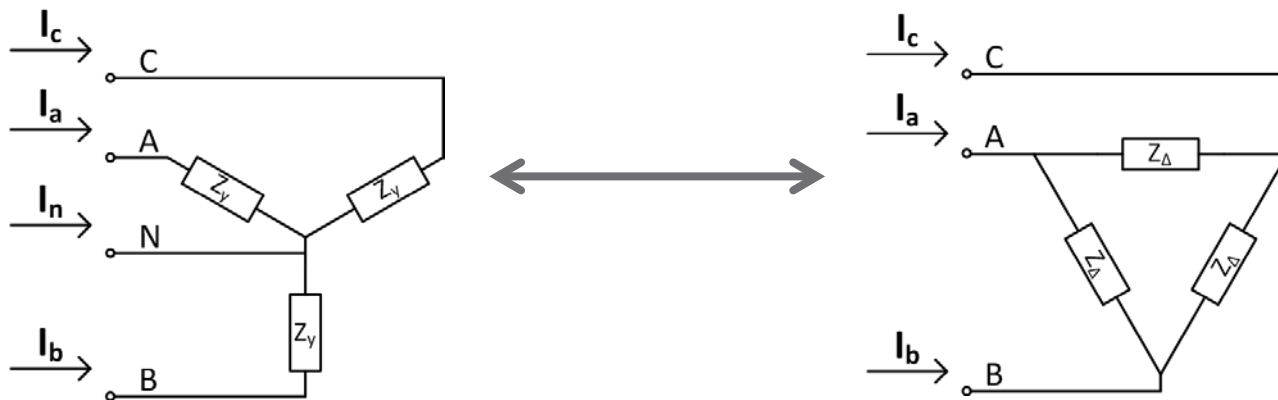
$$I_b = \frac{3V_{LN}\angle -120^\circ}{Z_{\Delta}} = \sqrt{3}I_{BC}\angle -30^\circ$$

$$I_c = \frac{3V_{LN}\angle 120^\circ}{Z_{\Delta}} = \sqrt{3}I_{CA}\angle -30^\circ$$

Δ – Y Conversion

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- Analysis is often simpler when dealing with Y -connected loads
 - ▣ Would like a way to convert Δ loads to Y loads (and vice versa)



- For a Y load and a Δ load to be equivalent, they must result in equal line currents

Δ – Y Conversion

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- Line currents for a Y -connected load:

$$I_a = \frac{V_{LN} \angle 0^\circ}{Z_Y}$$

$$I_b = \frac{V_{LN} \angle -120^\circ}{Z_Y}$$

$$I_c = \frac{V_{LN} \angle 120^\circ}{Z_Y}$$

- For a Δ -connected load:

$$I_a = \frac{3V_{LN} \angle 0^\circ}{Z_\Delta}$$

$$I_b = \frac{3V_{LN} \angle -120^\circ}{Z_\Delta}$$

$$I_c = \frac{3V_{LN} \angle 120^\circ}{Z_\Delta}$$

$\Delta - Y$ Conversion

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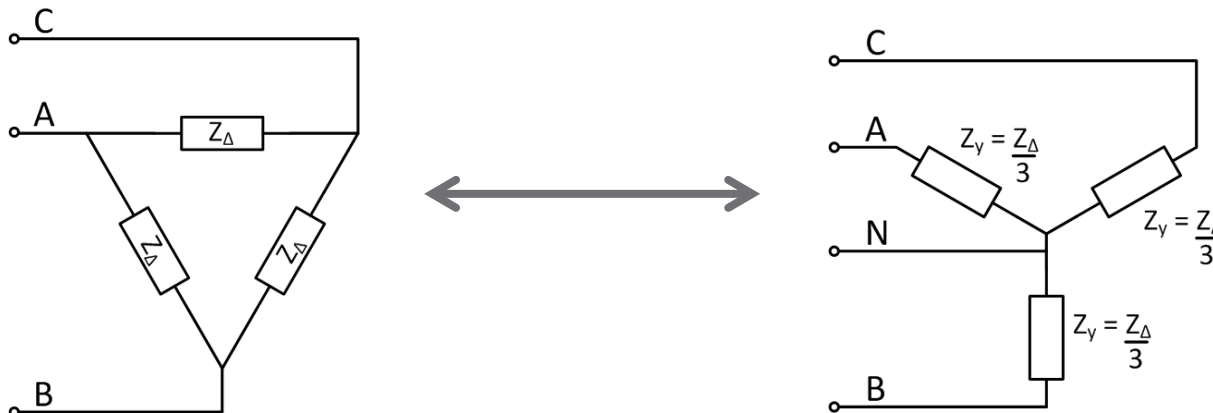
- Equating any of the three line currents, we can determine the impedance relationship

$$\frac{V_{LN} \angle 0^\circ}{Z_Y} = \frac{3V_{LN} \angle 0^\circ}{Z_\Delta}$$

$$Z_Y = \frac{Z_\Delta}{3}$$

and

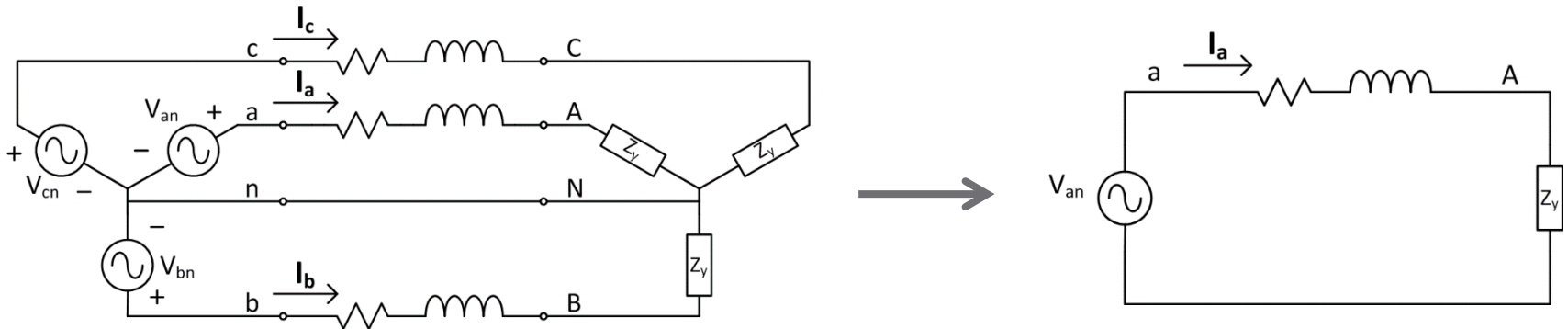
$$Z_\Delta = 3Z_Y$$



Line-to-Neutral Schematics

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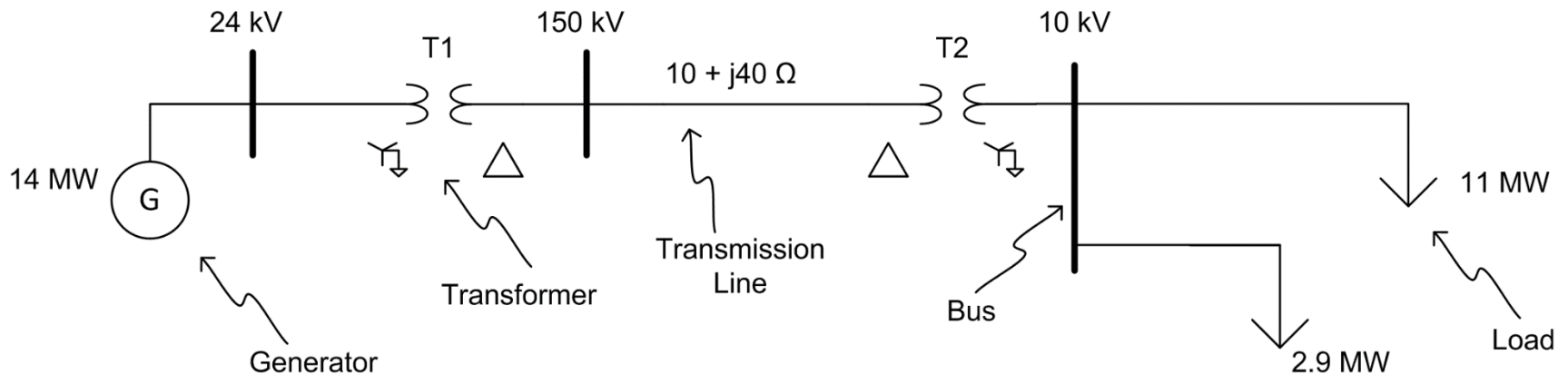
- For balanced networks, we can simplify our analysis by considering only a single phase
 - ▣ A ***per-phase analysis***
 - ▣ Other phases are simply shifted by $\pm 120^\circ$
- For example, a balanced Y - Y circuit:



One-Line Diagrams

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- Power systems are often depicted using ***one-line diagrams*** or ***single-line diagrams***
 - ▣ Not a schematic – not all wiring is shown
- For example:

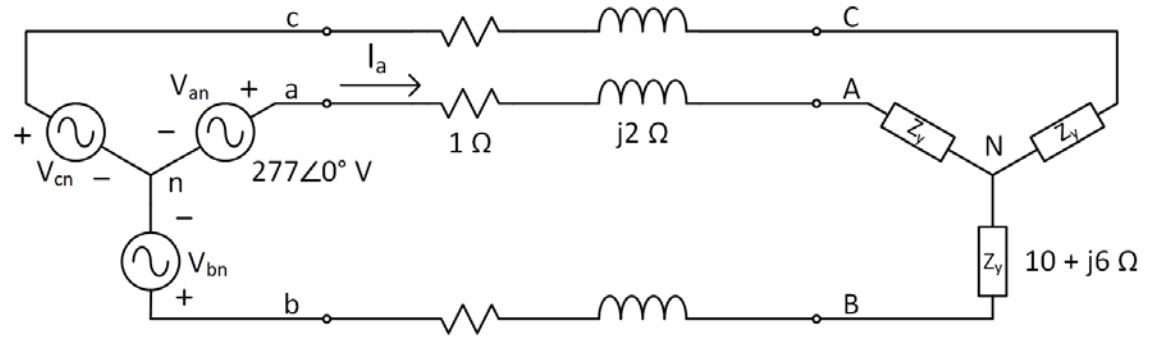


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Example Problems

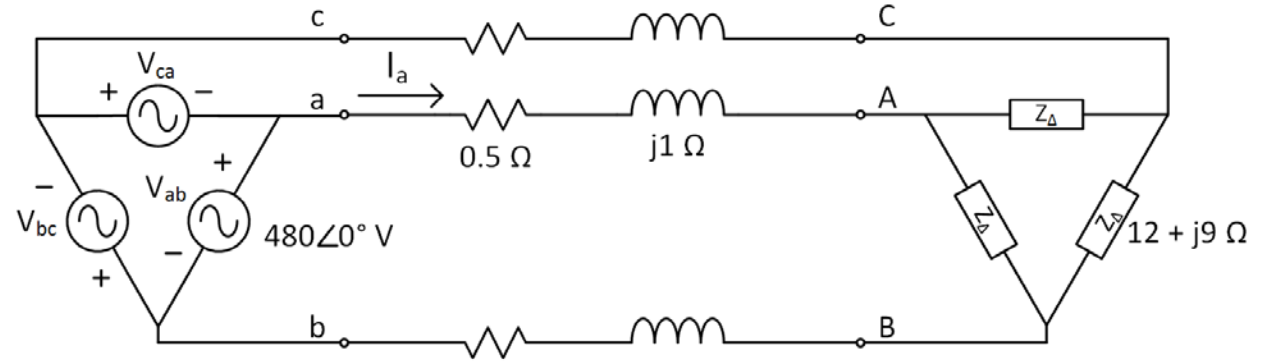
Determine:

- ▣ I_a
- ▣ V_{AN}
- ▣ V_{AB}



Determine:

- ▣ I_a
- ▣ V_{AB}
- ▣ V_{AN}
- ▣ V_{BC}

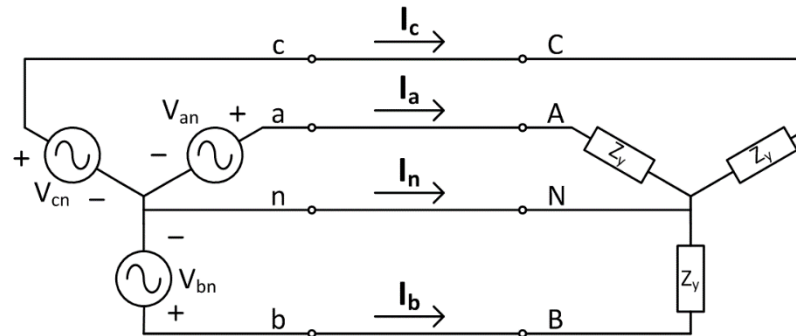


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Power in Balanced 3ϕ Networks

Instantaneous Power

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- We'll first determine the instantaneous power supplied by the source
 - ▣ Neglecting line impedance, this is also the power absorbed by the load
- The phase a line-to-neutral voltage is

$$v_{an}(t) = \sqrt{2}V_{LN} \cos(\omega t + \delta)$$

- The phase a current is

$$i_a(t) = \sqrt{2}I_L \cos(\omega t + \beta)$$

where β depends on the load impedance

Instantaneous Power

- The instantaneous power delivered out of phase a of the source is

$$p_a(t) = v_{an}(t)i_a(t)$$

$$p_a(t) = 2V_{LN}I_L \cos(\omega t + \delta) \cos(\omega t + \beta)$$

$$p_a(t) = V_{LN}I_L \cos(\delta - \beta) + V_{LN}I_L \cos(2\omega t + \delta + \beta)$$

- The b and c phases are shifted by $\pm 120^\circ$
 - ▣ Power from each of these phases is

$$p_b(t) = V_{LN}I_L \cos(\delta - \beta) + V_{LN}I_L \cos(2\omega t + \delta + \beta - 240^\circ)$$

$$p_c(t) = V_{LN}I_L \cos(\delta - \beta) + V_{LN}I_L \cos(2\omega t + \delta + \beta + 240^\circ)$$

Instantaneous Power

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- The *total* power delivered by the source is the sum of the power from each phase

$$p_{3\phi}(t) = p_a(t) + p_b(t) + p_c(t)$$

$$p_{3\phi}(t) = 3V_{LN}I_L \cos(\delta - \beta) \\ + V_{LN}I_L [\cos(2\omega t + \delta + \beta) \\ + \cos(2\omega t + \delta + \beta - 240^\circ) \\ + \cos(2\omega t + \delta + \beta + 240^\circ)]$$

- Everything in the square brackets cancels, leaving

$$p_{3\phi}(t) = 3V_{LN}I_L \cos(\delta - \beta) = P_{3\phi}$$

- **Power in a balanced 3 ϕ network is constant**
- In terms of line-to-line voltages, the power is

$$P_{3\phi} = \sqrt{3}V_{LL}I_L \cos(\delta - \beta)$$

Complex Power

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- The **complex power** delivered by phase a is

$$\mathbf{S}_a = \mathbf{V}_{an}\mathbf{I}_a^* = V_{LN}\angle\delta(I_L\angle\beta)^*$$

$$\mathbf{S}_a = V_{LN}I_L\angle(\delta - \beta)$$

$$\mathbf{S}_a = V_{LN}I_L \cos(\delta - \beta) + jV_{LN}I_L \sin(\delta - \beta)$$

- For phase b , complex power is

$$\mathbf{S}_b = \mathbf{V}_{bn}\mathbf{I}_b^* = V_{LN}\angle(\delta - 120^\circ)(I_L\angle(\beta - 120^\circ))^*$$

$$\mathbf{S}_b = V_{LN}I_L\angle(\delta - \beta)$$

$$\mathbf{S}_b = V_{LN}I_L \cos(\delta - \beta) + jV_{LN}I_L \sin(\delta - \beta)$$

- This is equal to \mathbf{S}_a and also to phase \mathbf{S}_c

Complex Power

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- The ***total complex power*** is

$$S_{3\phi} = S_a + S_b + S_c$$

$$S_{3\phi} = 3V_{LN}I_L \angle(\delta - \beta)$$

$$S_{3\phi} = 3V_{LN}I_L \cos(\delta - \beta) + j3V_{LN}I_L \sin(\delta - \beta)$$

- The ***apparent power*** is the magnitude of the complex power

$$S_{3\phi} = 3V_{LN}I_L$$

Complex Power

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- Complex power can be expressed in terms of the real and reactive power

$$\mathbf{S}_{3\phi} = P_{3\phi} + jQ_{3\phi}$$

- The **real power**, as we've already seen is

$$P_{3\phi} = 3V_{LN}I_L \cos(\delta - \beta)$$

- The **reactive power** is

$$Q_{3\phi} = 3V_{LN}I_L \sin(\delta - \beta)$$

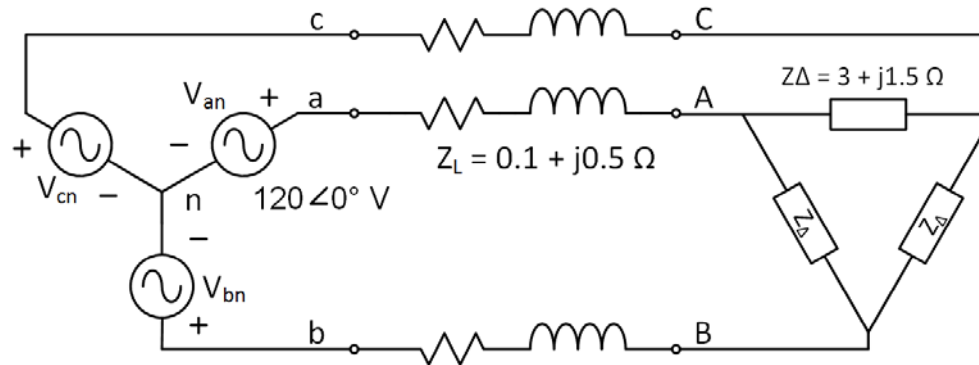
Advantages of Three-Phase Power

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- Advantages of three-phase power:
 - For a given amount of power, ***half the amount of wire required*** compared to single-phase
 - No return current on neutral conductor
 - ***Constant real power***
 - Constant motor torque
 - Less noise and vibration of machinery

Three-Phase Power – Example

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- Determine
 - ▣ Load voltage, V_{AB}
 - ▣ Power triangle for the load
 - ▣ Power factor at the load

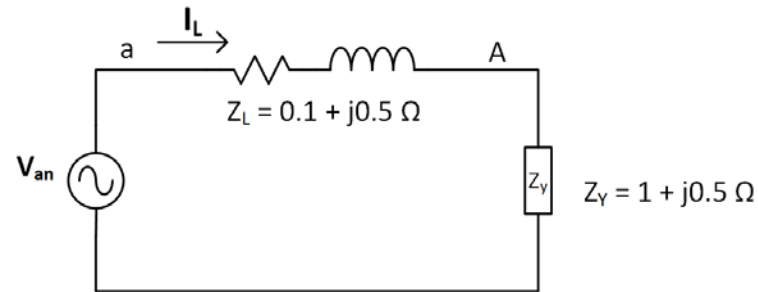
- We'll do a per-phase analysis, so first convert the Δ load to a Y load

$$Z_Y = \frac{Z_{\Delta}}{3} = 1 + j0.5 \Omega$$

Three-Phase Power – Example

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- The per-phase circuit:



- The line current is

$$I_L = \frac{V_{an}}{Z_L + Z_Y} = \frac{120 \angle 0^\circ V}{1.1 + j1 \Omega} = \frac{120 \angle 0^\circ V}{1.45 \angle 42.3^\circ \Omega}$$

$$I_L = 80.7 \angle -42.3^\circ A$$

- The line-to-neutral voltage at the load is

$$V_{AN} = I_L Z_Y = (80.7 \angle -42.3^\circ A)(1 + j0.5 \Omega)$$

$$V_{AN} = (80.7 \angle -42.3^\circ A)(1.12 \angle 26.6^\circ \Omega)$$

$$V_{AN} = 90.25 \angle -15.71^\circ V$$

Three-Phase Power – Example

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- Calculate the line-to-line voltage from the line-to-neutral voltage

$$V_{AB} = \sqrt{3}V_{AN}\angle 30^\circ$$

$$V_{AB} = 156\angle 14.3^\circ V$$

- Alternatively, we could calculate line-to-line voltage from the two line-to-neutral voltages.
 - The line-to-neutral voltage at phase B is

$$V_{BN} = 90.25\angle -135.71^\circ V$$

- So the line-to-line voltage is given by

$$V_{AB} = V_{AN} - V_{BN} = 156\angle 14.3^\circ V$$

Three-Phase Power – Example

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- The complex power absorbed by the load is

$$\mathbf{S}_{3\phi} = 3\mathbf{S}_A = 3V_{AN}I_L^*$$

$$\mathbf{S}_{3\phi} = 3(90.25\angle -15.71^\circ V)(80.7\angle -42.3^\circ A)^*$$

$$\mathbf{S}_{3\phi} = 21.85 \angle 26.6^\circ \text{ kVA}$$

$$\mathbf{S}_{3\phi} = 19.53 + j9.78 \text{ kVA}$$

- The apparent power:

$$S_{3\phi} = 21.85 \text{ kVA}$$

- Real power:

$$P = 19.53 \text{ kW}$$

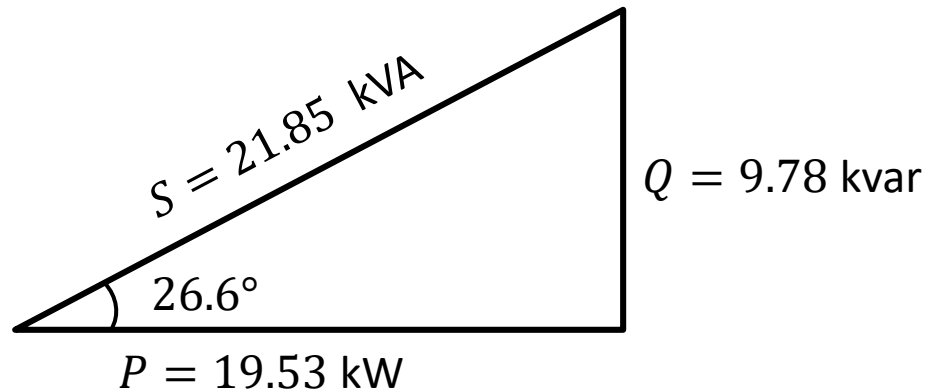
- Reactive power:

$$Q = 9.78 \text{ kvar}$$

Three-Phase Power – Example

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- The power triangle at the load:



- The power factor at the load is

$$p.f. = \cos(26.6^\circ) = \frac{P}{S} = \frac{19.53 \text{ kW}}{21.85 \text{ kVA}}$$

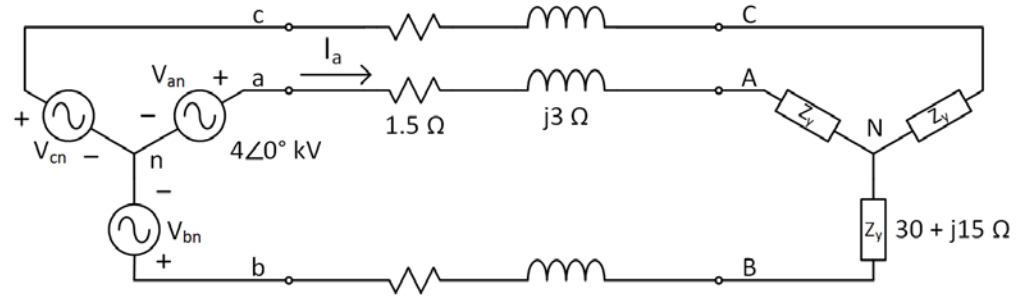
$$p.f. = 0.89 \text{ lagging}$$

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Example Problems

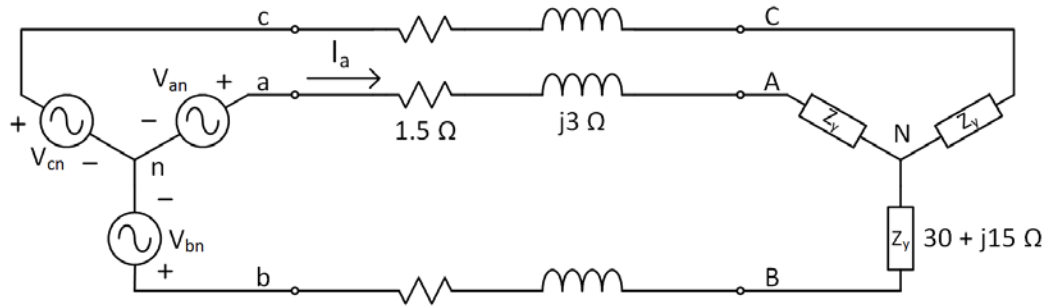
Determine complex power:

- From the source
- To the load
- To the line



Line-to-line voltage at the load is maintained at 4.16 kV.

What is the voltage at the source? How much complex power is delivered by the source?



Line-to-line voltage at the load is maintained at 4.16 kV.

Determine:

- Power factor at load
- Power triangle at load
- Loss in Lines

