## SECTION 3: INVERSE LAPLACE TRANSFORMS

ENGR 203 - Electrical Fundamentals III

## Inverse Laplace Transform

We've just seen how time-domain functions can be transformed to the Laplace domain. Next, we'll look at how we can solve differential equations in the Laplace domain and transform back to the time domain.

## Laplace Transforms - Differential Equations

$\square$ Consider the simple RLC circuit from the introductory section of notes:
$\square$ The governing differential
 equation is

$$
\frac{d^{2} v_{O}}{d t^{2}}+\frac{R}{L} \frac{d v_{O}}{d t}+\frac{1}{L C} v_{o}(t)=\frac{1}{L C} v_{i}(t)
$$

$\square$ Or, using dot notation

$$
\begin{equation*}
\ddot{v}_{o}(t)+\frac{R}{L} \dot{v}_{o}(t)+\frac{1}{L C} v_{o(t)}=\frac{1}{L C} v_{i}(t) \tag{1}
\end{equation*}
$$

## Laplace Transforms - Differential Equations

$\square$ We'll now use Laplace transforms to determine the step response of the system

- 1 V step input

$$
v_{i}(t)=1 V \cdot u(t)= \begin{cases}0 V, & t<0  \tag{2}\\ 1 V, & t \geq 0\end{cases}
$$


$\square$ For the step response, we assume zero initial conditions

$$
\begin{equation*}
v_{o}(0)=0 \text { and } \dot{v}_{o}(0)=0 \tag{3}
\end{equation*}
$$

$\square$ Using the derivative property of the Laplace transform, (1) becomes

$$
\begin{align*}
& s^{2} V_{o}(s)-s v_{o}(0)-\dot{v}_{o}(0)+\frac{R}{L} s V_{o}(s)-\frac{R}{L} v_{o}(0)+\frac{1}{L C} V_{o}(s)=\frac{1}{L C} V_{i}(s) \\
& s^{2} V_{o}(s)+\frac{R}{L} s V_{o}(s)+\frac{1}{L C} V_{o}(s)=\frac{1}{L C} V_{i}(s) \tag{4}
\end{align*}
$$

## Laplace Transforms - Differential Equations

$\square$ The input is a step, so (4) becomes

$$
\begin{equation*}
s^{2} V_{o}(s)+\frac{R}{L} s V_{o}(s)+\frac{1}{L C} V_{o}(s)=\frac{1}{L C} \frac{1}{s} \tag{5}
\end{equation*}
$$

$\square$ Solving (5) for $V_{o}(s)$

$$
\begin{align*}
& V_{o}(s)\left(s^{2}+\frac{R}{L} s+\frac{1}{L C}\right)=\frac{1}{L C} \frac{1}{s} \\
& V_{o}(s)=\frac{1 / L C}{s\left(s^{2}+\frac{R}{L} s+\frac{1}{L C}\right)} \tag{6}
\end{align*}
$$

$\square$ Equation (6) is the solution to the differential equation of (1), given the step input and I.C.'s

- The system step response in the Laplace domain
- Next, we need to transform back to the time domain


## Laplace Transforms - Differential Equations

$$
\begin{equation*}
V_{O}(s)=\frac{1 / L C}{s\left(s^{2}+\frac{R}{L} s+\frac{1}{L C}\right)} \tag{6}
\end{equation*}
$$


$\square$ The form of (6) is typical of Laplace transforms when dealing with linear systems

- A rational polynomial in $s$
- Here, the numerator is $0^{\text {th }}$-order

$$
V_{o}(s)=\frac{B(s)}{A(s)}
$$

$\square$ Roots of the numerator polynomial, $B(s)$, are called the zeros of the function
$\square$ Roots of the denominator polynomial, $A(s)$, are called the poles of the function

## Inverse Laplace Transforms

$$
\begin{equation*}
V_{o}(s)=\frac{1 / L C}{s\left(s^{2}+\frac{R}{L} s+\frac{1}{L C}\right)} \tag{6}
\end{equation*}
$$

$\square$ To get (6) back into the time domain, we need to perform an inverse Laplace
 transform

- An integral inverse transform exists, but we don't use it
- Instead, we use partial fraction expansion
$\square$ Partial fraction expansion
- Idea is to express the Laplace transform solution, (6), as a sum of Laplace transform terms that appear in the table
- Procedure depends on the type of roots of the denominator polynomial
- Real and distinct
- Repeated
- Complex


## Inverse Laplace Transforms - Example 1

$\square$ Consider the following system parameters

$$
\begin{aligned}
& R=25 \Omega \\
& L=10 \mu H \\
& C=100 \mathrm{nF}
\end{aligned}
$$


$\square$ Laplace transform of the step response becomes

$$
\begin{equation*}
V_{o}(s)=\frac{1 E 12}{s\left(s^{2}+2.5 E 6 s+1 E 12\right)} \tag{7}
\end{equation*}
$$

$\square$ Factoring the denominator

$$
\begin{equation*}
V_{o}(s)=\frac{1 E 12}{s(s+500 E 3)(s+2 E 6)} \tag{8}
\end{equation*}
$$

$\square$ In this case, the denominator polynomial has three real, distinct roots:

$$
s_{1}=0, \quad s_{2}=-500 E 3, \quad s_{3}=-2 E 6
$$

## Inverse Laplace Transforms - Example 1

- Partial fraction expansion of (8) has the form

$$
\begin{equation*}
V_{o}(s)=\frac{1 E 12}{s(s+500 E 3)(s+2 E 6)}=\frac{r_{1}}{s}+\frac{r_{2}}{s+500 E 3}+\frac{r_{3}}{s+2 E 6} \tag{9}
\end{equation*}
$$



- The numerator coefficients, $r_{1}, r_{2}$, and $r_{3}$, are called residues
$\square$ Can already see the form of the time-domain function
- Sum of a constant and two decaying exponentials
$\square$ To determine the residues, multiply both sides of (9) by the denominator of the left-hand side

$$
\begin{aligned}
& 1 E 12=r_{1}(s+500 E 3)(s+2 E 6)+r_{2} s(s+2 E 6)+r_{3} s(s+500 E 3) \\
& 1 E 12=r_{1} s^{2}+2.5 E 6 r_{1} s+1 E 12 r_{1}+r_{2} s^{2}+2 E 6 r_{2} s+r_{3} s^{2}+500 E 3 r_{3} s
\end{aligned}
$$

$\square$ Collecting terms, we have

$$
\begin{equation*}
1 E 12=s^{2}\left(r_{1}+r_{2}+r_{3}\right)+s\left(2.5 E 6 r_{1}+2 E 6 r_{2}+500 E 3 r_{3}\right)+1 E 12 r_{1} \tag{10}
\end{equation*}
$$

## Inverse Laplace Transforms - Example 1

$\square$ Equating coefficients of powers of $s$ on both sides of (10) gives a system of three equations in three unknowns

$$
\begin{array}{ll}
s^{2}: & 0=r_{1}+r_{2}+r_{3} \\
s^{1}: & 0=2.5 E 6 r_{1}+2 E 6 r_{2}+500 E 3 r_{3} \\
s^{0}: & 1 E 12=1 E 12 r_{1}
\end{array}
$$


$\square$ Solving for the residues gives

$$
\begin{aligned}
& r_{1}=1 \\
& r_{2}=-1.333 \\
& r_{3}=0.333
\end{aligned}
$$

$\square$ The Laplace transform of the step response is

$$
\begin{equation*}
V_{o}(s)=\frac{1}{s}-\frac{1.333}{s+500 E 3}+\frac{0.333}{s+2 E 6} \tag{11}
\end{equation*}
$$

$\square$ Equation (11) can now be transformed back to the time domain using the Laplace transform table

## Inverse Laplace Transforms - Example 1

$\square$ The time-domain step response of the system is the sum of a constant term and two decaying exponentials:

$$
\begin{equation*}
v_{o}(t)=1 V-1.333 V e^{-500 E 3 t}+0.333 V e^{-2 E 6 t} \tag{12}
\end{equation*}
$$

$\square$ Step response plotted in MATLAB
$\square$ Characteristic of a signal having only real poles

- No overshoot/ringing
$\square$ Steady-state voltage agrees with intuition



## Inverse Laplace Transforms - Example 1

$\square$ Go back to (7) and apply the initial value theorem
$v_{o}(0)=\lim _{s \rightarrow \infty} s V_{o}(s)=\lim _{s \rightarrow \infty} \frac{1 E 12}{\left(s^{2}+2.5 E 6 s+1 E 12\right)}=0 \mathrm{~V}$

$\square$ Which is, in fact our assumed initial condition
$\square$ Next, apply the final value theorem to the Laplace transform step response, (7)

$$
\begin{aligned}
& v_{o}(\infty)=\lim _{s \rightarrow 0} s V_{o}(s)=\lim _{s \rightarrow 0} \frac{1 E 12}{\left(s^{2}+2.5 E 6 s+1 E 12\right)} \\
& v_{o}(\infty)=\frac{1 E 12}{1 E 12}=1 \mathrm{~V}
\end{aligned}
$$

$\square$ This final value agrees with both intuition and our numerical analysis

## Inverse Laplace Transforms - Example 2

$\square$ Reduce the resistance and re-calculate the step response

$$
\begin{aligned}
& R=20 \Omega \\
& L=10 \mu H \\
& C=100 n F
\end{aligned}
$$


$\square$ Laplace transform of the step response becomes

$$
\begin{equation*}
V_{o}(s)=\frac{1 E 12}{s\left(s^{2}+2 E 6 s+1 E 12\right)} \tag{13}
\end{equation*}
$$

$\square$ Factoring the denominator

$$
\begin{equation*}
V_{o}(s)=\frac{1 E 12}{s(s+1 E 6)^{2}} \tag{14}
\end{equation*}
$$

$\square$ In this case, the denominator polynomial has three real roots, two of which are identical

$$
s_{1}=0, \quad s_{2}=-1 E 6, \quad s_{3}=-1 E 6
$$

## Inverse Laplace Transforms - Example 2

$\square$ Partial fraction expansion of (14) has the form

$$
\begin{equation*}
V_{o}(s)=\frac{1 E 12}{s(s+1 E 6)^{2}}=\frac{r_{1}}{s}+\frac{r_{2}}{s+1 E 6}+\frac{r_{3}}{(s+1 E 6)^{2}} \tag{15}
\end{equation*}
$$


$\square$ Again, find residues by multiplying both sides of (15) by the lefthand side denominator

$$
\begin{aligned}
& 1 E 12=r_{1}(s+1 E 6)^{2}+r_{2} s(s+1 E 6)+r_{3} s \\
& 1 E 12=r_{1} s^{2}+2 E 6 r_{1} s+1 E 12 r_{1}+r_{2} s^{2}+1 E 6 r_{2} s+r_{3} s
\end{aligned}
$$

$\square$ Collecting terms, we have

$$
\begin{equation*}
1 E 12=s^{2}\left(r_{1}+r_{2}\right)+s\left(2 E 6 r_{1}+1 E 6 r_{2}+r_{3}\right)+1 E 12 r_{1} \tag{16}
\end{equation*}
$$

## Inverse Laplace Transforms - Example 2

$\square$ Equating coefficients of powers of $s$ on both sides of (16) gives a system of three equations in three unknowns

$$
\begin{array}{ll}
s^{2}: & 0=r_{1}+r_{2} \\
s^{1}: & 0=2 E 6 r_{1}+1 E 6 r_{2}+r_{3} \\
s^{0}: & 1 E 12=1 E 12 r_{1}
\end{array}
$$


$\square$ Solving for the residues gives

$$
\begin{aligned}
& r_{1}=1 \\
& r_{2}=-1 \\
& r_{3}=-1 E 6
\end{aligned}
$$

$\square \quad$ The Laplace transform of the step response is

$$
\begin{equation*}
V_{o}(s)=\frac{1}{s}-\frac{1}{s+1 E 6}-\frac{1 E 6}{(s+1 E 6)^{2}} \tag{17}
\end{equation*}
$$

$\square$ Equation (17) can now be transformed back to the time domain using the Laplace transform table

## Inverse Laplace Transforms - Example 2

$\square$ The time-domain step response of the system is the sum of a constant, a decaying exponential, and a decaying exponential scaled by time:

$$
\begin{equation*}
v_{o}(t)=1 V-1 V e^{-1 E 6 t}-1 E 6 \frac{V}{s} t e^{-1 E 6 t} \tag{18}
\end{equation*}
$$

- Step response plotted in MATLAB
$\square$ Again, characteristic of a signal having only real poles
- Similar to the last case
- A bit faster - slower pole at $s=-500 E 3$ was eliminated

Step Response


## Inverse Laplace Transforms - Example 3

$\square$ Reduce the resistance even further and go through the process once again

$$
\begin{aligned}
& R=10 \Omega \\
& L=10 \mu H \\
& C=100 n F
\end{aligned}
$$


$\square$ Laplace transform of the step response becomes

$$
\begin{equation*}
V_{o}(s)=\frac{1 E 12}{s\left(s^{2}+1 E 6 s+1 E 12\right)} \tag{19}
\end{equation*}
$$

$\square$ The second-order term in the denominator now has complex roots, so we won't factor any further
$\square$ The denominator polynomial still has a root at zero and now has two roots which are a complex-conjugate pair

$$
s_{1}=0, \quad s_{2}=-500 E 3+j 866 E 3, \quad s_{3}=-500 E 3-j 866 E 3
$$

## Inverse Laplace Transforms - Example 3

$\square$ Want to cast the partial fraction terms into forms that appear in the Laplace transform table
$\square$ Second-order terms should be of the form

$$
\begin{equation*}
\frac{r_{i}(s+\sigma)+r_{i+1} \omega}{(s+\sigma)^{2}+\omega^{2}} \tag{20}
\end{equation*}
$$

$\square$ This will transform into the sum of damped sine and cosine terms

$$
\mathcal{L}^{-1}\left\{r_{i} \frac{(s+\sigma)}{(s+\sigma)^{2}+\omega^{2}}+r_{i+1} \frac{\omega}{(s+\sigma)^{2}+\omega^{2}}\right\}=r_{i} e^{-\sigma t} \cos (\omega t)+r_{i+1} e^{-\sigma t} \sin (\omega t)
$$

$\square$ To get the second-order term in the denominator of (19) into the form of (20), complete the square, to give the following partial fraction expansion

$$
\begin{equation*}
V_{o}(s)=\frac{1 E 12}{s\left(s^{2}+1 E 6 s+1 E 12\right)}=\frac{r_{1}}{s}+\frac{r_{2}(s+500 E 3)+r_{3}(866 E 3)}{(s+500 E 3)^{2}+(866 E 3)^{2}} \tag{21}
\end{equation*}
$$

## Inverse Laplace Transforms - Example 3

$\square$ Note that the $\sigma$ and $\omega$ terms in (20) and (21) are the real and imaginary parts of the complex-conjugate denominator roots

$$
s_{2,3}=-\sigma \pm j \omega=-500 E 3 \pm j 866 E 3
$$


$\square$ Multiplying both sides of (21) by the left-hand-side denominator, equate coefficients and solve for residues as before:

$$
\begin{aligned}
& r_{1}=1 \\
& r_{2}=-1 \\
& r_{3}=-0.577
\end{aligned}
$$

$\square$ Laplace transform of the step response is

$$
\begin{equation*}
V_{o}(s)=\frac{1}{s}-\frac{(s+500 E 3)}{(s+500 E 3)^{2}+(866 E 3)^{2}}-\frac{0.577(866 E 3)}{(s+500 E 3)^{2}+(866 E 3)^{2}} \tag{22}
\end{equation*}
$$

## Inverse Laplace Transforms - Example 3

$\square$ The time-domain step response of the system is the sum of a constant and two decaying sinusoids:

$$
\begin{equation*}
y(t)=1 V-1 V e^{-500 E 3 t} \cos (866 E 3 t)-0.577 V e^{-500 E 3 t} \sin (866 E 3 t) \tag{23}
\end{equation*}
$$

$\square$ Step response and individual components plotted in MATLAB
$\square$ Characteristic of a signal having complex poles

- Sinusoidal terms result in overshoot and (possibly) ringing

Step Response


## Laplace-Domain Signals with Complex Poles

$\square$ The Laplace transform of the step response in the last example had complex poles

- A complex-conjugate pair: $s=-\sigma \pm j \omega$

$\square$ Much more on this later


# Natural \& Driven Responses 

## Natural and Forced Responses


$\square$ In the previous section we used Laplace transforms to determine the response of a circuit to a step input, given zero initial conditions

- The driven response
$\square$ Now, consider the response of the same system to non-zero initial conditions only
- The natural response


## Natural Response

$\square$ Same under-damped RLC circuit

- Now the input steps from 1 V to 0 V at $t=0$

$$
v_{i}(t)=1 V-1 V u(t)
$$


$\square$ Since $v_{i}(t \geq 0)=0$, the governing equation becomes

$$
\begin{equation*}
\ddot{v}_{o}+\frac{R}{L} \dot{v}_{o}+\frac{1}{L C} v_{o}=0 \tag{24}
\end{equation*}
$$

$\square$ Use the derivative property to Laplace transform (24)

- Allow for non-zero initial-conditions

$$
\begin{equation*}
s^{2} V_{o}(s)-s v_{o}(0)-\dot{v}_{o}(0)+\frac{R}{L} s V_{o}(s)-\frac{R}{L} v_{o}(0)+\frac{1}{L C} V_{o}(s)=0 \tag{25}
\end{equation*}
$$

## Natural Response

$\square$ Solving (25) for $V_{o}(s)$ gives the Laplace transform of the output due solely to initial conditions

- Laplace transform of the natural response

$$
\begin{equation*}
V_{o}(s)=\frac{s v_{o}(0)+\dot{v}_{o}(0)+\frac{R}{L} v_{o}(0)}{s^{2}+\frac{R}{L} s+\frac{1}{L C}} \tag{26}
\end{equation*}
$$

$\square$ For the given input, for $t<0$ :

- $v_{i}(t<0)=1 \mathrm{~V}$
- $i(t<0)=0 A$
- $v_{o}(t<0)=1 \mathrm{~V}$
$\square$ At $t=0$, neither $i(t)$ nor $v_{o}(t)$ can change instantaneously, so the initial conditions are:

$$
v_{o}(0)=1 \mathrm{~V} \quad \text { and } \quad \dot{v}_{o}(0)=0 \mathrm{~V} / \mathrm{s}
$$

## Natural Response

$\square$ Substituting component parameters and initial conditions into (26)

$$
\begin{equation*}
V_{o}(s)=\frac{s+1 E 6}{\left(s^{2}+1 E 6 s+1 E 12\right)} \tag{27}
\end{equation*}
$$

$\square$ Remember, it's the roots of the denominator polynomial that dictate the form of the response

- Real roots - decaying exponentials
- Complex roots - decaying sinusoids
$\square$ For the under-damped case, roots are complex
- Complete the square
- Partial fraction expansion has the form

$$
\begin{equation*}
V_{o}(s)=\frac{s+1 E 6}{\left(s^{2}+1 E 6 s+1 E 12\right)}=\frac{r_{1}(s+500 E 3)+r_{2}(866 E 3)}{(s+500 E 3)^{2}+(866 E 3)^{2}} \tag{28}
\end{equation*}
$$

## Natural Response

$$
\begin{equation*}
V_{o}(s)=\frac{s+1 E 6}{\left(s^{2}+1 E 6 s+1 E 12\right)}=\frac{r_{1}(s+500 E 3)+r_{2}(866 E 3)}{(s+500 E 3)^{2}+(866 E 3)^{2}} \tag{28}
\end{equation*}
$$

$\square$ Multiply both sides of (28) by the denominator of the left-hand side

$$
s+1 E 6=r_{1} s+500 E 3 r_{1}+866 E 3 r_{2}
$$

$\square$ Equating coefficients and solving for $r_{1}$ and $r_{2}$ gives

$$
r_{1}=1, r_{2}=0.577
$$

$\square$ The Laplace transform of the natural response:

$$
\begin{equation*}
V_{o}(s)=\frac{(s+500 E 3)}{(s+500 E 3)^{2}+(866 E 3)^{2}}+\frac{0.577(866 E 3)}{(s+500 E 3)^{2}+(866 E 3)^{2}} \tag{29}
\end{equation*}
$$

## Natural Response

$\square$ Inverse Laplace transform is the natural response

$$
\begin{equation*}
y(t)=1 V e^{-500 E 3 t} \cos (866 E 3 \cdot t)+0.577 V e^{-500 E 3 t} \sin (866 E 3 \cdot t) \tag{30}
\end{equation*}
$$

$\square$ Under-damped response is the sum of decaying sine and cosine terms


## Driven Response with Non-Zero I.C.s

$\square$ Now, change the source to provide both non-zero input (for $t \geq 0$ ) and non-zero initial conditions:

$$
v_{i}(t)=-1 V+2 V \cdot u(t)
$$


$\square$ The Laplace transform of the output including both input and initial conditions:

$$
s^{2} V_{o}(s)-s v_{o}(0)-\dot{v}_{o}(0)+\frac{R}{L} s V_{o}(s)-\frac{R}{L} v_{o}(0)+\frac{1}{L C} V_{o}(s)=\frac{1}{L C} V_{i}(s)
$$

$\square$ Solving for $V_{o}(s)$ gives

$$
\begin{equation*}
V_{o}(s)=\frac{s v_{o}(0)+\dot{v}_{o}(0)+\frac{R}{L} v_{o}(0)+\frac{1}{L C} V_{i}(s)}{s^{2}+\frac{R}{L} s+\frac{1}{L C}} \tag{3}
\end{equation*}
$$

## Driven Response with Non-Zero I.C.'s

$\square$ Laplace transform of the response has two components

$$
\begin{equation*}
V_{O}(s)=\underbrace{\frac{s v_{o}(0)+\dot{v}_{O}(0)+\frac{R}{L} v_{o}(0)}{\left(s^{2}+\frac{R}{L} s+\frac{1}{L C}\right)}}+\underbrace{\frac{\frac{1}{L C} F_{i n}(s)}{\left(s^{2}+\frac{R}{L} s+\frac{1}{L C}\right)}} \tag{32}
\end{equation*}
$$

Natural response - initial conditions
Driven response - input
$\square$ Total response is a superposition of the initial condition response and the driven response
$\square$ Both have the same denominator polynomial

- Same roots, same type of response
- Over-, under-, critically-damped


## Driven Response with Non-Zero I.C.s

$\square$ The input now is

$$
v_{i}(t)=-1 V+2 V \cdot u(t)= \begin{cases}-1 V & t<0 \\ +1 V & t \geq 0\end{cases}
$$

$\square$ For $t \geq 0$, the input is $1 V$

- The same as a unit step, so it's Laplace transform is simply

$$
V_{i}(s)=\frac{1}{s}
$$

$\square$ The fact that $v_{i}(t<0)=-1 V$ is accounted for by the initial conditions:

$$
v_{o}(0)=-1 \mathrm{~V} \text { and } \quad \dot{v}_{o}(0)=0 \mathrm{~V} / \mathrm{s}
$$

## Driven Response with Non-Zero I.C.'s

$\square$ Substituting in component and input values gives the Laplace transform of the total response

$$
V_{o}(s)=\frac{-s-1 E 6+\frac{1 E 12}{s}}{\left(s^{2}+1 E 6 s+1 E 12\right)}=\frac{-s^{2}-1 E 6 s+1 E 12}{s\left(s^{2}+1 E 6 s+1 E 12\right)}
$$

$\square$ Transform back to time domain via partial fraction expansion

$$
V_{o}(s)=\frac{r_{1}}{s}+\frac{r_{2}(s+500 E 3)}{(s+500 E 3)^{2}+(866 E 3)^{2}}+\frac{r_{3}(866 E 3)}{(s+500 E 3)^{2}+(866 E 3)^{2}}
$$

$\square$ Solving for the residues gives

$$
r_{1}=1, \quad r_{2}=-2, \quad r_{3}=-1.15
$$

## Driven Response with Non-Zero I.C.'s

$\square$ Total response:

$$
v_{o}(t)=1-2 e^{-500 E 3 t} \cos (866 E 3 \cdot t)-1.15 e^{-500 E 3 t} \sin (866 E 3 \cdot t)
$$

$\square$ Superposition of two components

- Natural response due to initial conditions
$\square$ Driven response due to the input


