# SECTION 3: INVERSE LAPLACE TRANSFORMS

ENGR 203 – Electrical Fundamentals III

#### 2

## Inverse Laplace Transform

We've just seen how time-domain functions can be transformed to the Laplace domain. Next, we'll look at how we can solve differential equations in the Laplace domain and transform back to the time domain.

- 3
- Consider the simple RLC circuit from the introductory section of notes:
- The governing differential equation is

$$\frac{d^2 v_o}{dt^2} + \frac{R}{L} \frac{dv_o}{dt} + \frac{1}{LC} v_o(t) = \frac{1}{LC} v_i(t)$$

Or, using dot notation

$$\ddot{v}_{o}(t) + \frac{R}{L}\dot{v}_{o}(t) + \frac{1}{LC}v_{o(t)} = \frac{1}{LC}v_{i}(t)$$
(1)



- 4
- We'll now use Laplace transforms to determine the *step response* of the system
- 1 V step input

$$v_i(t) = 1 V \cdot u(t) = \begin{cases} 0 V, \ t < 0 \\ 1 V, \ t \ge 0 \end{cases}$$

□ For the step response, we assume *zero initial conditions* 

$$v_o(0) = 0$$
 and  $\dot{v}_o(0) = 0$  (3)

□ Using the derivative property of the Laplace transform, (1) becomes

$$s^{2}V_{o}(s) - sv_{o}(0) - \dot{v}_{o}(0) + \frac{R}{L}sV_{o}(s) - \frac{R}{L}v_{o}(0) + \frac{1}{LC}V_{o}(s) = \frac{1}{LC}V_{i}(s)$$

$$s^{2}V_{o}(s) + \frac{R}{L}sV_{o}(s) + \frac{1}{LC}V_{o}(s) = \frac{1}{LC}V_{i}(s)$$
(4)

 $em \xrightarrow{i(t)} R \xrightarrow{L} v_o(t)$   $v_i(t) \xrightarrow{r} 1V \cdot u(t) \xrightarrow{r} C$  (2)

5

The input is a step, so (4) becomes

$$s^{2}V_{o}(s) + \frac{R}{L}sV_{o}(s) + \frac{1}{LC}V_{o}(s) = \frac{1}{LC}\frac{1}{s}$$

□ Solving (5) for  $V_o(s)$ 

$$V_{o}(s)\left(s^{2} + \frac{R}{L}s + \frac{1}{LC}\right) = \frac{1}{LC}\frac{1}{s}$$
$$V_{o}(s) = \frac{1/LC}{s\left(s^{2} + \frac{R}{L}s + \frac{1}{LC}\right)}$$
(6)

(5) v<sub>i</sub>(t) 1V·u(t)

R

- Equation (6) is the solution to the differential equation of (1), given the step input and I.C.'s
  - The system step response in the Laplace domain
  - Next, we need to transform back to the time domain

 $v_o(t)$ 

$$V_o(s) = \frac{1/LC}{s\left(s^2 + \frac{R}{L}s + \frac{1}{LC}\right)}$$

- (6)  $\xrightarrow{I(t)} R \qquad L \qquad v_o(t)$  $v_i(t) \qquad IV \cdot u(t) \qquad C$
- The form of (6) is typical of Laplace transforms when dealing with linear systems
  - A rational polynomial in s
  - Here, the numerator is 0<sup>th</sup>-order

$$V_o(s) = \frac{B(s)}{A(s)}$$

- Roots of the numerator polynomial, B(s), are called the zeros of the function
- Roots of the denominator polynomial, A(s), are called the **poles** of the function

## Inverse Laplace Transforms

$$V_o(s) = \frac{1/LC}{s\left(s^2 + \frac{R}{L}s + \frac{1}{LC}\right)}$$

 To get (6) back into the time domain, we need to perform an *inverse Laplace transform*



• An integral inverse transform exists, but we don't use it

■ Instead, we use *partial fraction expansion* 

#### Partial fraction expansion

- Idea is to express the Laplace transform solution, (6), as a sum of Laplace transform terms that appear in the table
- Procedure depends on the type of roots of the denominator polynomial
  - Real and distinct
  - Repeated
  - Complex

8

Consider the following system parameters

$$R = 25 \Omega$$

$$L = 10 \ \mu H$$

C = 100 nF



Laplace transform of the step response becomes

$$V_0(s) = \frac{1E12}{s(s^2 + 2.5E6s + 1E12)}$$
(7)

Factoring the denominator

$$V_o(s) = \frac{1E12}{s(s+500E3)(s+2E6)}$$
(8)

 In this case, the denominator polynomial has three *real, distinct roots*:

$$s_1 = 0, \qquad s_2 = -500E3, \qquad s_3 = -2E6$$

- 9
- Partial fraction expansion of (8) has the form

$$V_0(s) = \frac{1E12}{s(s+500E3)(s+2E6)} = \frac{r_1}{s} + \frac{r_2}{s+500E3} + \frac{r_3}{s+2E6}$$



- The numerator coefficients, r<sub>1</sub>, r<sub>2</sub>, and r<sub>3</sub>, are called *residues*
- Can already see the form of the time-domain function
   Sum of a *constant* and *two decaying exponentials*
- To determine the residues, multiply both sides of (9) by the denominator of the left-hand side

 $1E12 = r_1(s + 500E3)(s + 2E6) + r_2s(s + 2E6) + r_3s(s + 500E3)$ 

 $1E12 = r_1s^2 + 2.5E6r_1s + 1E12r_1 + r_2s^2 + 2E6r_2s + r_3s^2 + 500E3r_3s$ 

□ Collecting terms, we have

 $1E12 = s^{2}(r_{1} + r_{2} + r_{3}) + s(2.5E6r_{1} + 2E6r_{2} + 500E3r_{3}) + 1E12r_{1}$ (10)

10

 Equating coefficients of powers of s on both sides of (10) gives a system of three equations in three unknowns

$$s^{2}: 0 = r_{1} + r_{2} + r_{3}$$
  
 $s^{1}: 0 = 2.5E6r_{1} + 2E6r_{2} + 500E3r_{3}$   
 $s^{0}: 1E12 = 1E12r_{1}$ 

Solving for the residues gives

$$r_1 = 1$$
  
 $r_2 = -1.333$   
 $r_3 = 0.333$ 

The Laplace transform of the step response is

$$V_o(s) = \frac{1}{s} - \frac{1.333}{s + 500E3} + \frac{0.333}{s + 2E6}$$
(11)

 Equation (11) can now be transformed back to the time domain using the Laplace transform table



**ENGR 203** 

- 11
- The time-domain step response of the system is the sum of a constant term and two decaying exponentials:

$$v_o(t) = 1 V - 1.333 V e^{-500E3t} + 0.333 V e^{-2E6t}$$

(12)

- Step response plotted in MATLAB
- Characteristic of a signal having *only real poles*
  - No overshoot/ringing
- Steady-state voltage agrees with intuition



- 12
- Go back to (7) and apply the *initial value theorem*
  - $v_o(0) = \lim_{s \to \infty} sV_o(s) = \lim_{s \to \infty} \frac{1E12}{(s^2 + 2.5E6s + 1E12)} = 0 V$

- $v_i(t) \xrightarrow{\Gamma} 1V \cdot u(t) \xrightarrow{R} \xrightarrow{L} v_o(t) \xrightarrow{V_o(t)} C$
- Which is, in fact our assumed initial condition
- Next, apply the *final value theorem* to the Laplace transform step response, (7)

$$v_o(\infty) = \lim_{s \to 0} sV_o(s) = \lim_{s \to 0} \frac{1E12}{(s^2 + 2.5E6s + 1E12)}$$
$$v_o(\infty) = \frac{1E12}{1E12} = 1V$$

This final value agrees with both intuition and our numerical analysis

K. Webb

13

Reduce the resistance and re-calculate the step response

$$R = 20 \Omega$$
$$L = 10 \mu H$$
$$C = 100 nF$$



□ Laplace transform of the step response becomes

$$V_o(s) = \frac{1E12}{s(s^2 + 2E6s + 1E12)}$$
(13)

Factoring the denominator

$$V_o(s) = \frac{1E12}{s(s+1E6)^2}$$
(14)

 In this case, the denominator polynomial has three *real roots*, two of which are *identical*

$$s_1 = 0, \qquad s_2 = -1E6, \qquad s_3 = -1E6$$

- 14
- Partial fraction expansion of (14) has the form



Again, find residues by multiplying both sides of (15) by the left-hand side denominator

> $1E12 = r_1(s + 1E6)^2 + r_2s(s + 1E6) + r_3s$  $1E12 = r_1s^2 + 2E6r_1s + 1E12r_1 + r_2s^2 + 1E6r_2s + r_3s$

Collecting terms, we have 

> $1E12 = s^{2}(r_{1} + r_{2}) + s(2E6r_{1} + 1E6r_{2} + r_{3}) + 1E12r_{1}$ (16)

- 15
- Equating coefficients of powers of s on both sides of (16) gives a system of three equations in three unknowns

$$s^{2}: 0 = r_{1} + r_{2}$$
  
 $s^{1}: 0 = 2E6r_{1} + 1E6r_{2} + r_{3}$   
 $s^{0}: 1E12 = 1E12r_{1}$ 

Solving for the residues gives

$$r_1 = 1$$
  
 $r_2 = -1$   
 $r_3 = -1E6$ 

The Laplace transform of the step response is

$$V_0(s) = \frac{1}{s} - \frac{1}{s+1E6} - \frac{1E6}{(s+1E6)^2}$$
(17)

 Equation (17) can now be transformed back to the time domain using the Laplace transform table



- 16
- The time-domain step response of the system is the sum of a constant, a decaying exponential, and a decaying exponential scaled by time:

$$v_o(t) = 1 V - 1 V e^{-1E6t} - 1E6 \frac{V}{s} t e^{-1E6t}$$
(18)

- Step response plotted in MATLAB
- Again, characteristic of a signal having *only real poles*
  - Similar to the last case
  - A bit faster slower pole at s = -500E3 was eliminated



- 17
- Reduce the resistance even further and go through the process once again

$$R = 10 \Omega$$
$$L = 10 \mu H$$
$$C = 100 nF$$



□ Laplace transform of the step response becomes

$$V_o(s) = \frac{1E12}{s(s^2 + 1E6s + 1E12)}$$
(19)

- The second-order term in the denominator now has *complex roots*, so we won't factor any further
- The denominator polynomial still has a root at zero and now has two roots which are a *complex-conjugate pair*

$$s_1 = 0$$
,  $s_2 = -500E3 + j866E3$ ,  $s_3 = -500E3 - j866E3$ 

- 18
- Want to cast the partial fraction terms into forms that appear in the Laplace transform table
- Second-order terms should be of the form



$$\frac{r_i(s+\sigma)+r_{i+1}\omega}{(s+\sigma)^2+\omega^2} \tag{20}$$

This will transform into the sum of *damped sine* and *cosine* terms

$$\mathcal{L}^{-1}\left\{r_i\frac{(s+\sigma)}{(s+\sigma)^2+\omega^2}+r_{i+1}\frac{\omega}{(s+\sigma)^2+\omega^2}\right\}=r_ie^{-\sigma t}\cos(\omega t)+r_{i+1}e^{-\sigma t}\sin(\omega t)$$

To get the second-order term in the denominator of (19) into the form of (20), *complete the square*, to give the following partial fraction expansion

$$V_o(s) = \frac{1E12}{s(s^2 + 1E6s + 1E12)} = \frac{r_1}{s} + \frac{r_2(s + 500E3) + r_3(866E3)}{(s + 500E3)^2 + (866E3)^2}$$
(21)

- 19
- Note that the σ and ω terms in (20) and
   (21) are the *real* and *imaginary parts* of the complex-conjugate denominator roots



 $s_{2,3} = -\sigma \pm j\omega = -500E3 \pm j866E3$ 

 Multiplying both sides of (21) by the left-hand-side denominator, equate coefficients and solve for residues as before:

$$r_1 = 1$$
  
 $r_2 = -1$   
 $r_3 = -0.57$ 

7

Laplace transform of the step response is

$$V_0(s) = \frac{1}{s} - \frac{(s+500E3)}{(s+500E3)^2 + (866E3)^2} - \frac{0.577(866E3)}{(s+500E3)^2 + (866E3)^2}$$
(22)

- 20
- The time-domain step response of the system is the sum of a constant and two decaying sinusoids:

 $\left| y(t) = 1 V - 1 V e^{-500E3t} \cos(866E3t) - 0.577 V e^{-500E3t} \sin(866E3t) \right|$ (23)

- Step response and individual components plotted in MATLAB
- Characteristic of a signal having *complex poles*
  - Sinusoidal terms result in overshoot and (possibly) ringing



## Laplace-Domain Signals with Complex Poles

- 21
- The Laplace transform of the step response in the last example had complex poles
  - **D** A complex-conjugate pair:  $s = -\sigma \pm j\omega$
- Results in sine and cosine terms in the time domain

 $Ae^{-\sigma t}\cos(\omega t) + Be^{-\sigma t}\sin(\omega t)$ 

- $\Box$  Imaginary part of the roots,  $\omega$ 
  - Frequency of oscillation of sinusoidal components of the signal
- $\square$  *Real part* of the roots,  $\sigma$ ,
  - Rate of decay of the sinusoidal components
- Much more on this later





## Natural and Forced Responses



- In the previous section we used Laplace transforms to determine the response of a circuit to a step input, given zero initial conditions
  - The *driven response*
- Now, consider the response of the same system to non-zero initial conditions only
  - The *natural response*

23

- Same under-damped RLC circuit
- Now the input steps from 1 V to 0 V at t = 0

 $v_i(t) = 1V - 1V u(t)$ 

□ Since  $v_i (t \ge 0) = 0$ , the governing equation becomes

$$\ddot{v}_o + \frac{R}{L}\dot{v}_o + \frac{1}{LC}v_o = 0$$
(24)

Use the derivative property to Laplace transform (24)
 Allow for non-zero initial-conditions

$$s^{2}V_{o}(s) - sv_{o}(0) - \dot{v}_{o}(0) + \frac{R}{L}sV_{o}(s) - \frac{R}{L}v_{o}(0) + \frac{1}{LC}V_{o}(s) = 0$$
(25)



ENGR 203

25

Solving (25) for V<sub>o</sub>(s) gives the Laplace transform of the output due solely to *initial conditions* Laplace transform of the *natural response*

$$V_o(s) = \frac{sv_o(0) + \dot{v}_o(0) + \frac{R}{L}v_o(0)}{s^2 + \frac{R}{L}s + \frac{1}{LC}}$$
(26)

□ For the given input, for t < 0:

**D** 
$$v_i(t < 0) = 1 V$$

$$\bullet i(t < 0) = 0 A$$

$$\bullet v_o(t < 0) = 1 V$$

□ At t = 0, neither i(t) nor  $v_o(t)$  can change instantaneously, so the initial conditions are:

$$v_o(0) = 1 V$$
 and  $\dot{v}_o(0) = 0 V/s$ 

 Substituting component parameters and initial conditions into (26)

$$V_o(s) = \frac{s + 1E6}{(s^2 + 1E6s + 1E12)}$$
(27)

- Remember, it's the roots of the denominator polynomial that dictate the form of the response
  - Real roots decaying exponentials
  - Complex roots decaying sinusoids
- □ For the under-damped case, roots are complex
  - Complete the square
  - Partial fraction expansion has the form

$$V_0(s) = \frac{s + 1E6}{(s^2 + 1E6s + 1E12)} = \frac{r_1(s + 500E3) + r_2(866E3)}{(s + 500E3)^2 + (866E3)^2}$$
(28)

$$V_0(s) = \frac{s + 1E6}{(s^2 + 1E6s + 1E12)} = \frac{r_1(s + 500E3) + r_2(866E3)}{(s + 500E3)^2 + (866E3)^2}$$

Multiply both sides of (28) by the denominator of the left-hand side

 $s + 1E6 = r_1s + 500E3r_1 + 866E3r_2$ 

 $\Box$  Equating coefficients and solving for  $r_1$  and  $r_2$  gives

$$r_1 = 1, r_2 = 0.577$$

The Laplace transform of the natural response:

$$V_o(s) = \frac{(s+500E3)}{(s+500E3)^2 + (866E3)^2} + \frac{0.577(866E3)}{(s+500E3)^2 + (866E3)^2}$$
(29)

#### Inverse Laplace transform is the *natural response*

 $y(t) = 1 \, V e^{-500E3t} \cos(866E3 \cdot t) + 0.577 \, V e^{-500E3t} \sin(866E3 \cdot t)$ (30)

 Under-damped response is the sum of *decaying sine and cosine* terms



## Driven Response with Non-Zero I.C.s

- 29
- □ Now, change the source to provide both *non-zero input* (for  $t \ge 0$ ) and *non-zero initial conditions*:

$$v_i(t) = -1 V + 2 V \cdot u(t)$$

$$v_{i}(t) \xrightarrow{I(t)} R \xrightarrow{L} v_{o}(t)$$

$$10\Omega \qquad 10\mu H$$

$$100nF \xrightarrow{C} C$$

The Laplace transform of the output including both input and initial conditions:

$$s^{2}V_{o}(s) - sv_{o}(0) - \dot{v}_{o}(0) + \frac{R}{L}sV_{o}(s) - \frac{R}{L}v_{o}(0) + \frac{1}{LC}V_{o}(s) = \frac{1}{LC}V_{i}(s)$$

• Solving for  $V_o(s)$  gives

$$V_o(s) = \frac{sv_o(0) + \dot{v}_o(0) + \frac{R}{L}v_o(0) + \frac{1}{LC}V_i(s)}{s^2 + \frac{R}{L}s + \frac{1}{LC}}$$
(31)

## Driven Response with Non-Zero I.C.'s

Laplace transform of the response has two components



- Total response is a superposition of the initial condition response and the driven response
- Both have the same denominator polynomial
  - Same roots, same type of response
    - Over-, under-, critically-damped

## Driven Response with Non-Zero I.C.s

The input now is

$$v_i(t) = -1 V + 2 V \cdot u(t) = \begin{cases} -1 V & t < 0 \\ +1 V & t \ge 0 \end{cases}$$

- $\Box \text{ For } t \geq 0, \text{ the input is } 1 V$ 
  - The same as a unit step, so it's Laplace transform is simply

$$V_i(s) = \frac{1}{s}$$

■ The fact that  $v_i(t < 0) = -1 V$  is accounted for by the initial conditions:

$$v_o(0) = -1 V$$
 and  $\dot{v}_o(0) = 0 V/s$ 

## Driven Response with Non-Zero I.C.'s

- 32
- Substituting in component and input values gives the Laplace transform of the *total* response

$$V_o(s) = \frac{-s - 1E6 + \frac{1E12}{s}}{(s^2 + 1E6s + 1E12)} = \frac{-s^2 - 1E6s + 1E12}{s(s^2 + 1E6s + 1E12)}$$

 Transform back to time domain via partial fraction expansion

$$V_o(s) = \frac{r_1}{s} + \frac{r_2(s + 500E3)}{(s + 500E3)^2 + (866E3)^2} + \frac{r_3(866E3)}{(s + 500E3)^2 + (866E3)^2}$$

Solving for the residues gives

$$r_1 = 1, r_2 = -2, r_3 = -1.15$$

## Driven Response with Non-Zero I.C.'s

#### Total response:

 $v_o(t) = 1 - 2e^{-500E3t}\cos(866E3 \cdot t) - 1.15e^{-500E3t}\sin(866E3 \cdot t)$ 

- Superposition of two components
  - Natural response due to initial conditions
  - Driven response due to the input

