### **SECTION 5: FLOW BATTERIES**

ESE 471 – Energy Storage Systems



### **Flow Batteries**

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- Flow batteries are electrochemical cells, in which the reacting substances are stored in electrolyte solutions external to the battery cell
  - Electrolytes are *pumped* through the cells
  - Electrolytes flow across the electrodes
  - Reactions occur *at* the electrodes
  - Electrodes do not undergo a physical change



### **Flow Batteries**

### Flow batteries comprise two components:

#### Electrochemical cell

- Conversion between chemical and electrical energy
- External electrolyte storage tanks
  - Energy storage



Source: EPRI

### Flow Battery Electrochemical Cell

- Electrochemical cell
  - Two half-cells separated by a proton-exchange membrane (PEM)
  - Each half-cell contains an *electrode* and an *electrolyte* 
    - Positive half-cell: cathode and catholyte
    - Negative half-cell: anode and anolyte
- Redox reactions occur in each half-cell to produce or consume electrons during charge/discharge
- Similar to fuel cells, but two main differences:
  Reacting substances are all in the liquid phase
  Rechargeable (secondary cells)

### **Cell Stacks**

- Open-circuit voltage of an individual cell in the range of 1 V ... 2 V
  Determined by the particular chemistry
- For higher terminal voltages, multiple cells are connected in series
  Electrolyte flows through cell stack in parallel
- Carbon felt electrodes
  - Porous high surface area
  - High conductivity
- Bipolar plates separate individual cells in the stack
  - Shared electrode between adjacent cells
  - Positive electrode for one cell, negative electrode for the neighbor
- Electrodes on the ends are the external electrodes for the stack





### **Flow Battery Characteristics**

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- Relatively low *specific power* and *specific energy* Best suited for fixed (non-mobile) utility-scale applications
- Energy storage capacity and power rating are decoupled
  - Cell stack properties and geometry determine power
  - Volume of electrolyte in external tanks determines energy storage capacity
  - Flow batteries can be tailored for an particular application
- Very *fast response times* < 1 msec</p>
  - Time to switch between full-power charge and full-power discharge
  - Typically limited by controls and power electronics

#### Potentially very *long discharge times*

■ 4 – 10 hours is common

### Flow batteries vs. Conventional Batteries

#### Advantages over conventional batteries

- Energy storage capacity and power rating are decoupled
- Long lifetime
  - Electrolytes do not degrade
  - Electrodes are unaltered during charge/discharge
- Self-cooling
  - Inherently liquid-cooled
- All cells in a stack supplied with the same electrolyte
  - All cell voltages are equal
  - Individual cells not susceptible to overcharge/undercharge
  - No need for cell balancing

### Flow batteries vs. Conventional Batteries

#### Advantages over conventional batteries (cont'd)

- Equal charge/discharge rates (power)
- Bipolar electrodes are possible
  - Convenient for cell stacking

#### Disadvantages over conventional batteries

- Higher initial cost
- Increased complexity associated with pumps and plumbing
- Lower specific energy and specific power

### **Flow Battery Applications**

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#### Peak shaving/load shifting

- Infrastructure upgrade deferral
- Arbitrage
- Long duration

#### Load following

- Potentially replace peaker plants
- Long duration

#### Integration of renewables

- Smooth fluctuating power from wind and solar
- Improve grid stability
- Short duration

#### Frequency or voltage regulation

- Accommodate short-term real and reactive power demands
- Short duration

### **Cost of Flow Batteries**

- Cost of storage devices usually reported as either \$/kW or \$/kWh
- The Electric Power Research Institute (EPRI) estimates the cost of energy storages systems with *three cost components*
  - Costs that scale with *power* capacity
  - Costs that scale with *energy* storage capacity
  - Fixed costs
- Total capital cost is given by

Capital Cost = 
$$P \cdot (scaled power cost)$$
  
+  $E \cdot (scaled energy cost)$   
+ (fixed cost)

### **Cost of Flow Batteries**

In 2007, the EPRI flow battery cost estimates were:

- Power: \$2300/kW
- Energy: \$300/kWh
- Fixed: \$250,000
- EPRI 2007 projections for 2013:
   Power: \$1250/kW
  - Energy: \$210/kWh
  - Fixed: \$280,000

#### Future Projections for Capital Cost of Vanadium Redox Battery Systems



# <sup>14</sup> Flow Battery Chemistry

### Flow Battery Chemistry

Several different chemistries used in flow batteries
 Most employ *redox* (oxidation-reduction) *reactions* Often referred to as redox flow batteries or RFBs

#### Redox reactions

- Chemical reactions pairing a reduction reaction with an oxidation reaction
- **Oxidation states** of reactants are changed

#### Reduction

- Gaining of electrons
- Oxidation state is decreased (reduced)

#### Oxidation

- Loss of electrons
- Oxidation state is increased

### Redox Flow Battery Chemistry

- Oxidation at one electrode corresponds to reduction at the other
  - Opposite reactions occur during charging and discharging

#### Charging:

- Current flows from anode to cathode
- Electrons flow from cathode to anode
- Reduction occurs in the anolyte

$$A^{n+} + e^- \to A^{(n-1)+}$$

Oxidation occurs in the catholyte

$$B^{m+} \to B^{(m+1)+} + e^-$$

### **Redox Flow Battery Chemistry**

### Discharging:

Current flows from cathode to anode
 Electrops flow from anode to esthede

Electrons flow from anode to cathode

Oxidation occurs in the anolyte

 $A^{(n-1)+} \rightarrow A^{n+} + e^-$ 

Reduction occurs in the catholyte

$$B^{(m+1)+} + e^- \to B^{m+}$$

### **Redox Couples**

- Different flow batteries use different *redox couples* Pairs of redox reactants dissolved in electrolyte solution
- Common redox couples
  - Vanadium/vanadium, V/V
  - Zinc/bromine, Zn/Br
  - Iron/chromium, Fe/Cr
  - Bromine/Sulfur, Br/S
- Most common is the vanadium redox flow battery or VRB

### Vanadium

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- Abundant
- Inexpensive
- Byproduct of many mining operations
- Vanadium can exist in four different oxidation states
  V<sup>2+</sup>, V<sup>3+</sup>, V<sup>4+</sup>, and V<sup>5+</sup>
- In VRB electrolytes:
  - $V^{4+}$  exists as  $VO^{2+}$
  - $V^{5+}$  exists as  $VO_2^+$
- Vanadium in a VRB is dissolved in either:
  - Sulfuric acid
  - Mixture of sulfate and chloride (developed and licensed by PNNL)

### Vanadium

□ Vanadium changes color as it changes oxidation state



Source: www.eenews.net, David Ferris

Vanadium flow batteries use only a single element in both half-cells
 Eliminates the problem of cross-contamination across the membrane

### **VRB** Reactions

At the anode (charging to the right):

$$V^{3+} + e^- \rightleftharpoons V^{2+}$$

□ At the cathode (charging to the right):

$$V0^{2+} + H_20 \rightleftharpoons VO_2^+ + 2H^+ + e^-$$

Anode half-cell standard potential

**D**  $E_{0a} = -0.26 V$ 

Cathode half-cell standard potential

**D**  $E_{0c} = 0.99 V$ 

Cell standard potential

**•**  $E_0 = 1.25 V$ 

- Cell potential given by the *Nernst equation* 
  - Nominal value often considered 1.4 V

### Proton-Exchange Membrane

 Half-cells separated by a *proton-exchange membrane* (PEM)

- Allows protons to flow
  - From catholyte to anolyte during charging
  - From anolyte to catholyte during discharging



Source: EPRI

# 23 Electrochemical Model

### **Electrochemical Model**

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- As is the case for most batteries, a complete electrochemical model for a VRB is very complex
- Electrochemical model describes the relationship between cell voltage and
  - State of charge (SOC)
  - Operating conditions
    - Current
    - Electrolyte flow rate
    - Temperature
  - Internal losses
  - Electrolyte concentrations

### **Open-Circuit Voltage**

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#### The open-circuit voltage as a function of SOC :



## Equivalent Circuit Model

- Simple RFB equivalent circuit model
  - Thévenin equivalent circuit
  - State-of-charge-dependent open-circuit voltage source
- The resistance models losses in the battery
  - Voltaic losses
    - Ohmic and ionic losses in the electrodes, electrolytes, and membrane



#### **Coulombic** (*Faradaic*) losses

Losses due to chemical side reactions

# 27 Mechanical Model

- The equivalent circuit model accounts for electrical and electrochemical behavior of the flow battery
  - Models electrical and electrochemical losses that affect efficiency
- Flow batteries require electrolyte to be *pumped* through the cell stack
  - Pumps require power
  - Pump power affects efficiency

Need a *fluid model* for the battery in order to understand how *mechanical losses* affect efficiency

- Power required to pump electrolyte through cell stack
- Pumping power is proportional to
  - Density of the fluid
  - Head loss through the system
  - Flow rate

$$P_{pump} = \rho g h Q = \Delta p Q \tag{1}$$

 Total power required by the pump is determined by the pump efficiency

$$P_{pump,in} = \frac{P_{pump}}{\eta_{pump}} \tag{2}$$

Pressure drop through the system includes pressure drops through both the piping and the cell stack

$$\Delta p = \Delta p_{pipe} + \Delta p_{stack} \tag{3}$$

 Pressure drop along the piping is the sum of frictional losses and minor losses

$$\Delta p_{pipe} = -\gamma \left( \Delta z + h_f + h_m \right) \tag{4}$$

where

 $\gamma$ : specific weight of the fluid ( $\gamma = \rho g$ )  $\Delta z$ : height differential along the pipe  $h_f$ : frictional losses  $h_m$ : minor losses

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- The *frictional losses* and *minor losses* are the sum of the losses along each section of pipe or from each fitting, valve, bend, etc.
  Given by the *Darcy-Weisbach equation*

$$h_{f,i} = f_i \frac{L_i V_i^2}{D_i 2g}$$
(5)

and

$$h_{m,i} = k_{L,i} \frac{V_i^2}{2g}$$
(6)

where

- $f_i$ : Darcy friction factor dependent on roughness, diameter, and Reynolds number
- $k_{L,i}$ : loss coefficient associated with each lossy feature (e.g. inlet, outlet, valves, bends, etc.)
- $L_i$ : length of section
- $D_i$ : diameter of section

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- Calculating pressure drop across the cell stack becomes much more complicated
  - Analytically intractable
  - Evaluate using computational fluid dynamics (CFD) simulation



- CFD used for cell stack design to ensure
  - Uniform electrolyte flow across electrodes
  - Minimal pressure drop through stack

# 33 Efficiency

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- We would like to derive an expression for the round-trip efficiency of the flow battery
  - Ratio of the *energy delivered from* the battery to the *energy delivered to* the battery

$$\eta_{rt} = \frac{E_{out}}{E_{in}} \cdot 100\% \tag{7}$$

The input energy, E<sub>in</sub>, is the electrical energy delivered to the battery terminals plus the energy delivered to the pumps

$$E_{in} = E_{in,b} + E_{pump,in} \tag{8}$$

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- The energy quantities in (8) are given by the integrals of the respective powers
  - **•** For the battery

$$E_{in,b} = \int_0^{t_c} P_b(t) \, dt$$

$$E_{in,b} = \int_0^{t_c} i_b(t) v_b(t) dt$$



where  $t_c$  is the charging time

 The pump runs and requires power during both charge and discharge, so,

$$E_{pump,in} = \int_0^{t_c + t_d} P_{pump,in}(t) dt \tag{10}$$

where  $P_{pump,in}$  is given by (2)

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Substituting (10) and (9) into (8), we have

$$E_{in} = \int_0^{t_c} i_b(t) v_b(t) dt + \int_0^{t_c + t_d} P_{pump,in}(t) dt$$
(11)

- Note that not all of *E<sub>in,b</sub>* is stored
  Some energy is lost in *R<sub>b</sub>*
- Stored energy is

$$E_{stored} = E_{in,b} - E_{R_{b,in}}$$
$$E_{stored} = \int_0^{t_c} i_b(t) v_b(t) dt - \int_0^{t_c} i_b^2(t) R_b dt$$
(12)

□ The energy output from the battery is equal to the stored energy minus losses in  $R_b$  as energy flows out of the battery

$$E_{out} = E_{stored} - E_{R_{b,out}} = E_{in,b} - E_{R_{b,in}} - E_{R_{b,out}}$$
$$E_{out} = \int_0^{t_c} i_b(t) v_b(t) dt - \int_0^{t_c+t_d} i_b^2(t) R_b dt$$
(13)

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Substituting (11) and (13) into (7), gives the roundtrip efficiency:

$$\eta_{rt} = \frac{\int_0^{t_c} i_b(t) v_b(t) dt - \int_0^{t_c+t_d} i_b^2(t) R_b dt}{\int_0^{t_c} i_b(t) v_b(t) dt + \int_0^{t_c+t_d} P_{pump,in}(t) dt}$$

(14)

This is round-trip efficiency at the terminals of the battery

DC-DC efficiency

**•** Typical values: 70% ... 85%

- More meaningful is AC-AC round-trip efficiency
  - Accounts for power conversion system
  - May include transformer losses as well

$$\eta_{rt,AC} = \eta_{rt,DC} \cdot \eta_{pcs}^2 \cdot \eta_{tf}^2$$

- $\square \eta_{rt,DC}$  is given by (14)
- Transformer loss typically ~1%
- **Typical values: 65% ... 75%**

### **Electrolyte Flow Rate**

Efficiency is determined, in part, by the amount of power consumed by the pumps

Pumping power dependent on *flow rate*:

$$P_{pump} = \Delta p \cdot Q$$

### Minimum required flow rate is a function of:

- Battery input/output power
  - Higher power requires higher flow rate
- State of charge
  - Higher flow rate for:
    - Charging at high SOC
    - Discharging at low SOC

### **Flow Rate**

- One approach to setting flow rate for a given power charge/discharge:
  - Set flow rate to the maximum value required during the charge/discharge cycle
- Better yet, adjust flow rate to optimize efficiency
  - Dynamically adjust flow rate to the minimum required value for the current operating point
  - Variable flow rate will be a function of
    - SOC
    - Battery current
  - Necessary to account for non-equilibrium (transient) concentration effects within the cell



## Castle Valley, UT

- PacifiCorp (Utah Power) service area
- Rattlesnake #22 feeder
  - 85 miles long
  - 25 kV
  - 10,957 kVA connected distribution transformers
  - Serves Moab and Castle Valley
  - At or over capacity during hot summer months
  - Customer complaints of poor power quality
- Environmentally, geologically pristine, sensitive area



Source: VRB Power Systems

### Castle Valley, UT – VRB

#### Vanadium redox flow battery

- VRB Power Systems, Inc.
- Installed between the two load centers on the long distribution feeder
- **D** Power: 250 kW and 250 kvar
- Energy storage: 2 MWh
- **Discharge time**: 8 hours
- **3800** sq. ft.
- HVAC system maintains temperature at 5 °C ... 40 °C
- Purpose of the battery: *asset deferral* Alternative would be to upgrade the feeder



### Castle Valley, UT – VRB



### Castle Valley, UT – VRB

- □ Battery provides:
  - Peak shaving
  - Voltage regulation



## Castle Valley, UT – Electrolyte Tanks

- Electrolyte storage tanks
  - Only two
    - Other systems use many
  - Fiberglass
  - 43' long × 9.5' diameter
  - **70,000** liters



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### Castle Valley, UT – Stacks

### Six cell stacks

- Three two-stack series combinations connected in parallel
- 100 cells per stack
  - Nominal stack voltage: 140 V



- Each stack can provide 42 kW continuously
  Brief bursts of 150 kW possible
- Nominal DC battery voltage: 280 V



### Castle Valley, UT – Power Conversion System

- □ 375 kVA transformer connects to 3-φ, 480 V bus
- Inverter includes AC-DC and DC-DC inverters
- 353 kVA
- 94% efficiency
- Power output: 250 kW and 250 kvar
  - Leading or lagging power factor



### Castle Valley, UT – HMI

#### Human-machine interface:



## Castle Valley, UT – Battery Operation

- 50
- Predetermined daily baseline charge/discharge profiles
  - Summer and Winter profiles
- Variable real/reactive power provided on top of baseline power for voltage regulation
- DC-DC efficiency: 78%
- AC-AC efficiency: 69%



## Turlock, CA – Fe/Cr Flow Battery

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- Battery purpose
  Integration of renewables
   Load shifting
- Fe/Cr flow battery
  250 kW charge/ discharge



Source: EnerVault

- □1MWh
- 4 hours of charge/ discharge
- EnerVault Corporation

### Turlock, CA – Fe/Cr Flow Battery

- Almond orchard
  - 150 kW solar PV array
  - 260 kW well pump for irrigation
- Nine 120-cell stacks
  - 30 kW each



### Turlock, CA – Fe/Cr Flow Battery

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#### Unlike most flow batteries, EnerVault connects cell stacks in series



### Pullman, WA – VRB

- Washington State University, Pullman, WA
  - Vanadium redox flow battery
  - Largest flow battery in North America or EU
  - **1** MW
  - **u** 4 MWh
  - UniEnergy Technologies
- Battery used for
  - Frequency regulation
     Voltage regulation



### Pullman, WA – VRB

### UET battery modules

- **G** 600 kW
- **2.2** MWh
- Five 20' shipping containers
- 20 MW per acre
- 40 MW per acre if double-stacked
- **□**~\$700/kWh
- **D** 65% ... 70% AC efficiency

